

# Heat Transfer in Polymers

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# Heat Transfer in Polymers - Summary

- Introduction
- Thermal Conductivity
- Heat Transfer Coefficient
- Industrial Demonstrations: Corus, Zotefoams
- Standards for Thermal Properties Measurement
- Outline of Heat Transfer Project 2005-08
- Summary
  
- AOB

## Heat transfer is:

- key to polymer processing
- still inadequately understood
- key to increasing throughput - process times dominated by the cooling phase
- significant in affecting product properties, e.g. warpage, inadequate melting, thermal degradation

# Aim of the project

- To help companies measure and model heat transfer in polymer processing
- To enable measurement of more accurate data and encourage the use of improved models for numerical simulation software
- This should lead to:
  - Right first time design
  - Reduce cycle times / higher productivity (faster processing)
  - Energy saving
  - Fewer failures in service
  - Reduce waste- e.g. reduce warpage and hot spots during processingResulting in reduced costs and improved quality

# Tasks in the DTI Project

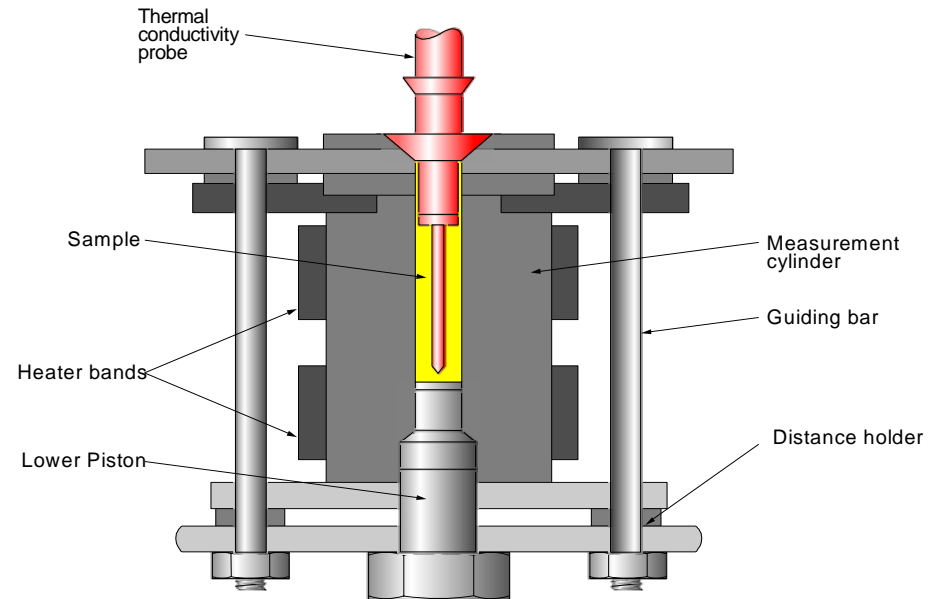
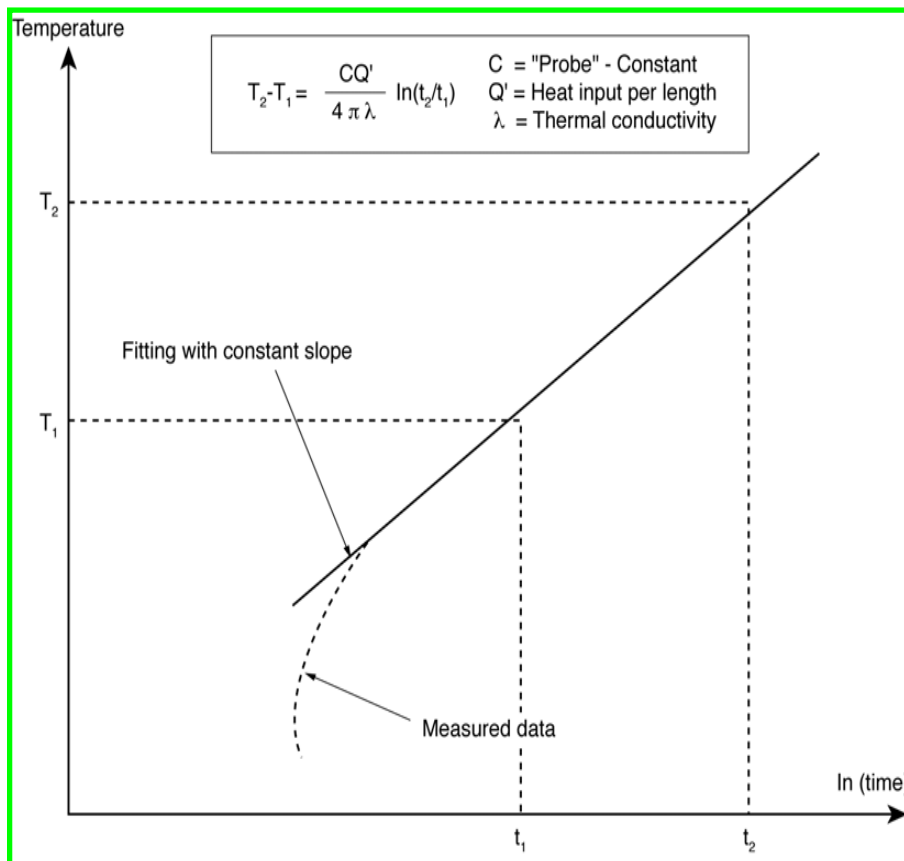
- Heat Transfer Coefficient
  - New facility
- Thermal Conductivity
  - Uncertainty analysis
  - Extension of method to new materials
- Simulation
  - To identify the important data
  - To help design equipment
  - Moldflow & NPL's own software
- Industrial Demonstrations
  - Zotefoams
  - Corus
- Dissemination
  - Web site, IAGs, PAA Newsletter articles, trade press articles, measurement notes, scientific paper

# Related Eureka Project: AIMTECH

- An associated Eureka project (AIMTECH) is progressing
- Its aim is to improve productivity of injection moulding
  - Main focus is on the moulds - reduce cycle times by using copper alloy moulds in injection moulding
- NPL Role
  - Measurement of the thermal conductivity of polymer melts (T,P)
  - Understanding the role of the mould/melt interface:  
Modelling heat transfer and the effect of uncertainties
- Six UK companies involved
- £25k co-funding contribution
- Close fit with the DTI project

# Thermal conductivity measurements

# Line source probe apparatus

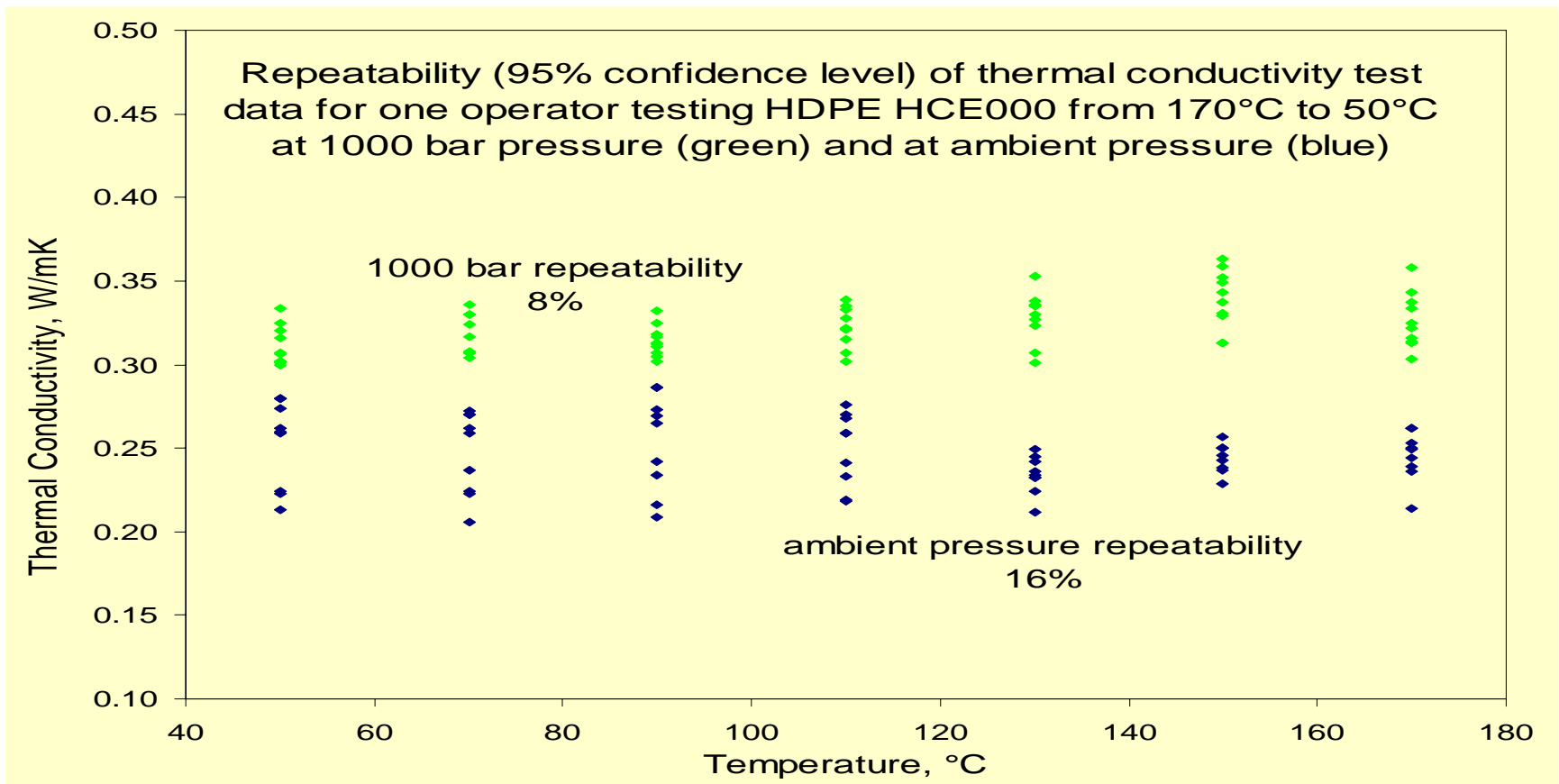


Measures thermal conductivity  
at industrially relevant  
processing pressures  
and temperatures



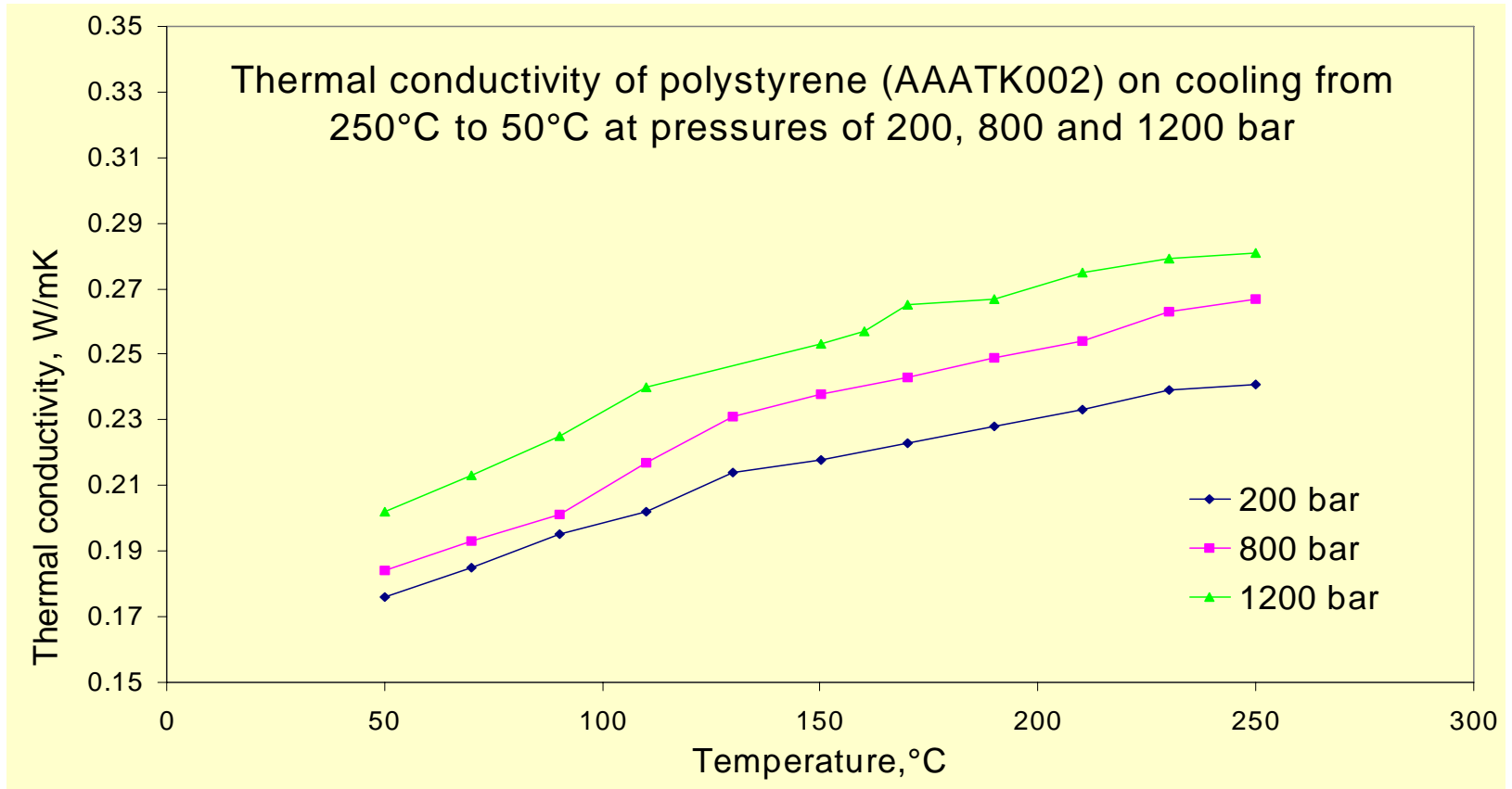
# Thermal conductivity

## HDPE at atmospheric pressure and 1000 bar

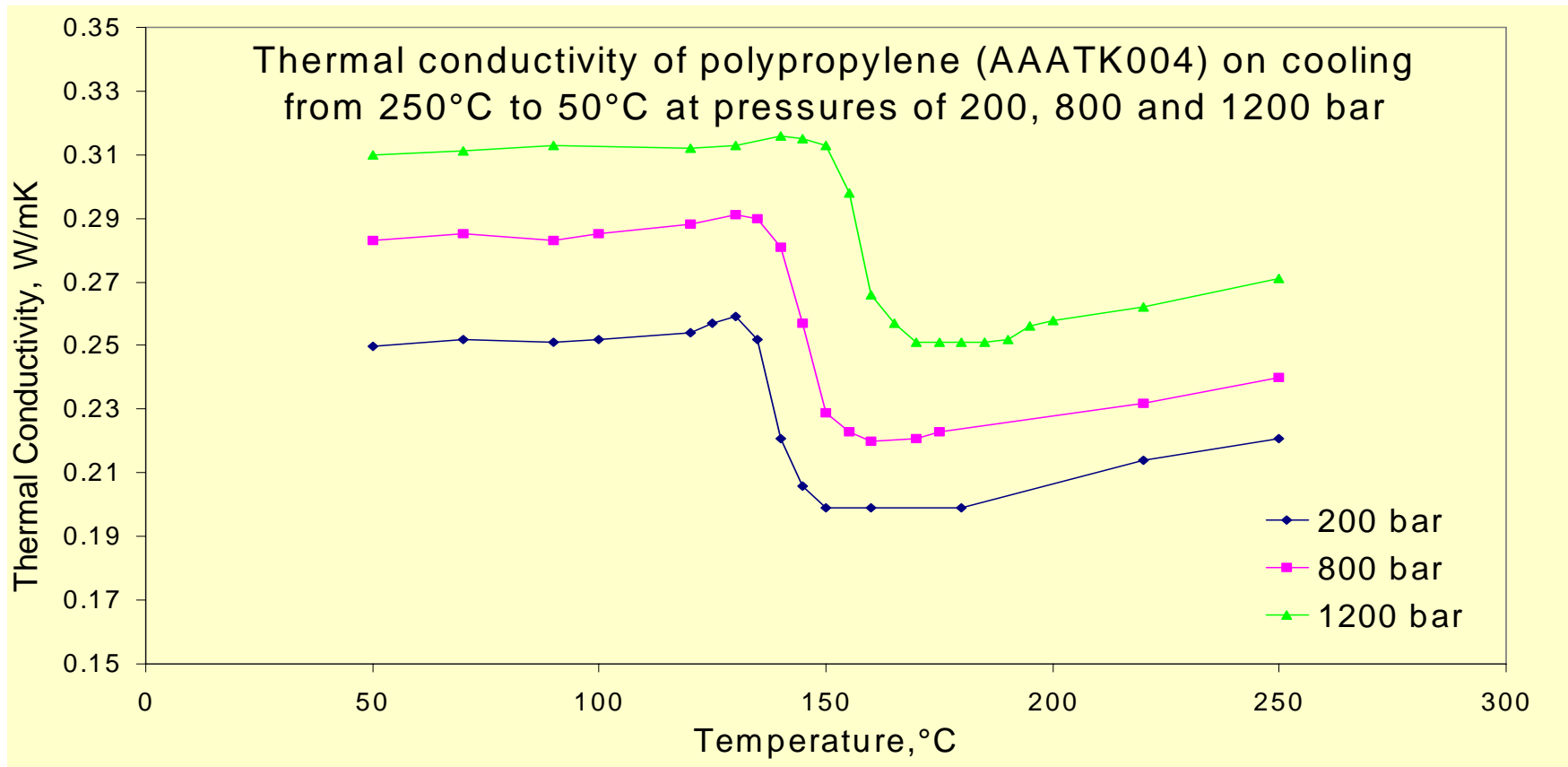


# Thermal conductivity

## Amorphous polystyrene (PS) under pressure



## Semi-crystalline polypropylene (PP) under pressure



# Thermal conductivity: implications of results

- Increase in pressure gives increase in thermal conductivity and increase in crystallisation temperature for semi-crystalline polymers
- Thermal conductivity data strongly dependent on both pressure and temperature:
  - 50% over range 50°C to 250°C
  - 43% over range 200 bar to 1200 barImplies single-point thermal conductivity value may be in error by up to 50%
- Important to use pressure and temperature dependent thermal conductivity data for accurate process modelling – will improve, for example, warpage and hot-spot prediction
- More accurate data based on industrial processing conditions - improvements in commercial modelling packages — possible cost benefits

# The Effect of Pressure on the Thermal Conductivity of Polymer Melts

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<http://www.npl.co.uk/materials/polyproc/iag>

**Heat transfer equipment  
for measurement of  
thermal conductivity  
and  
heat transfer coefficient**

# Heat Transfer Coefficient

- It is the heat flux per unit area ( $q$ ) across an interface from one material of temperature  $T_1$  to another material of temperature  $T_2$  :

$$h = q/(T_1 - T_2)$$

units:  $\text{Wm}^{-2}\text{K}^{-1}$

- Boundary condition for process simulation
- In injection moulding & compression moulding
  - Polymer to metal
  - Polymer-air-metal (GASM, ...)
- In extrusion & film blowing
  - Polymer to fluid (eg air or water)
- This project has built apparatus to measure heat transfer coefficient and will investigate the significance of different interfaces to commercial processing

# Heat Transfer Coefficient (heat transfer across an interface)

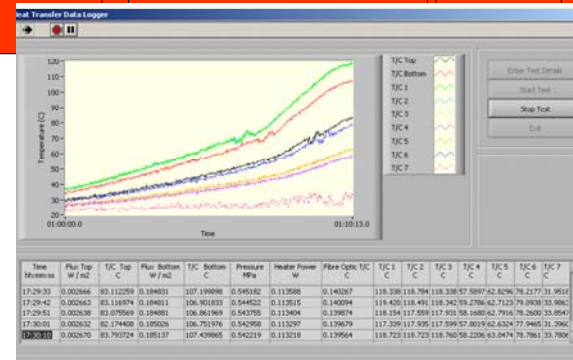
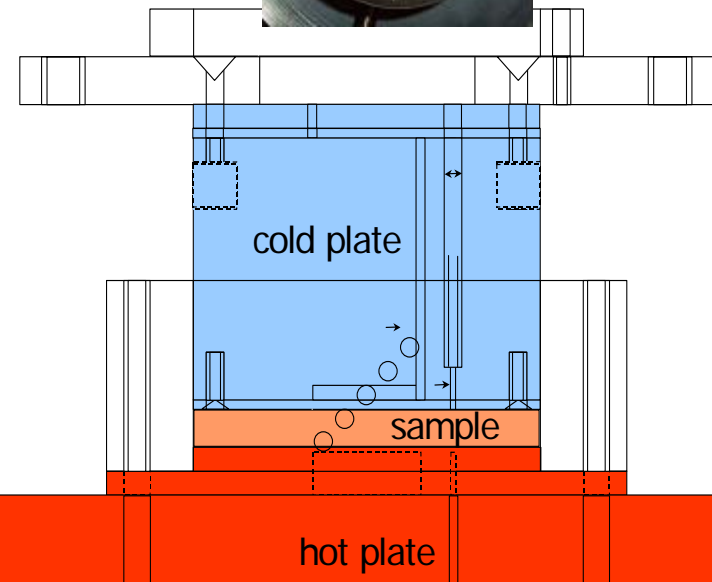
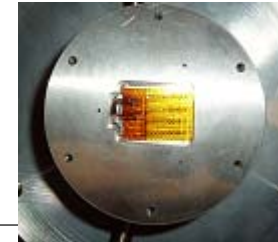
## Features of apparatus

- Room temperature to 275 °C, pressure to at least 500 bar
- Polymer samples 2 mm to 25 mm thick
- Interchangeable top plate to investigate
  - Different surface finishes
  - Effect of mould release agents
- Option to introduce a gap between polymer & top plate
  - Shrinkage, sink marks
- Instrumented with temperature measurement devices and heat flux sensors

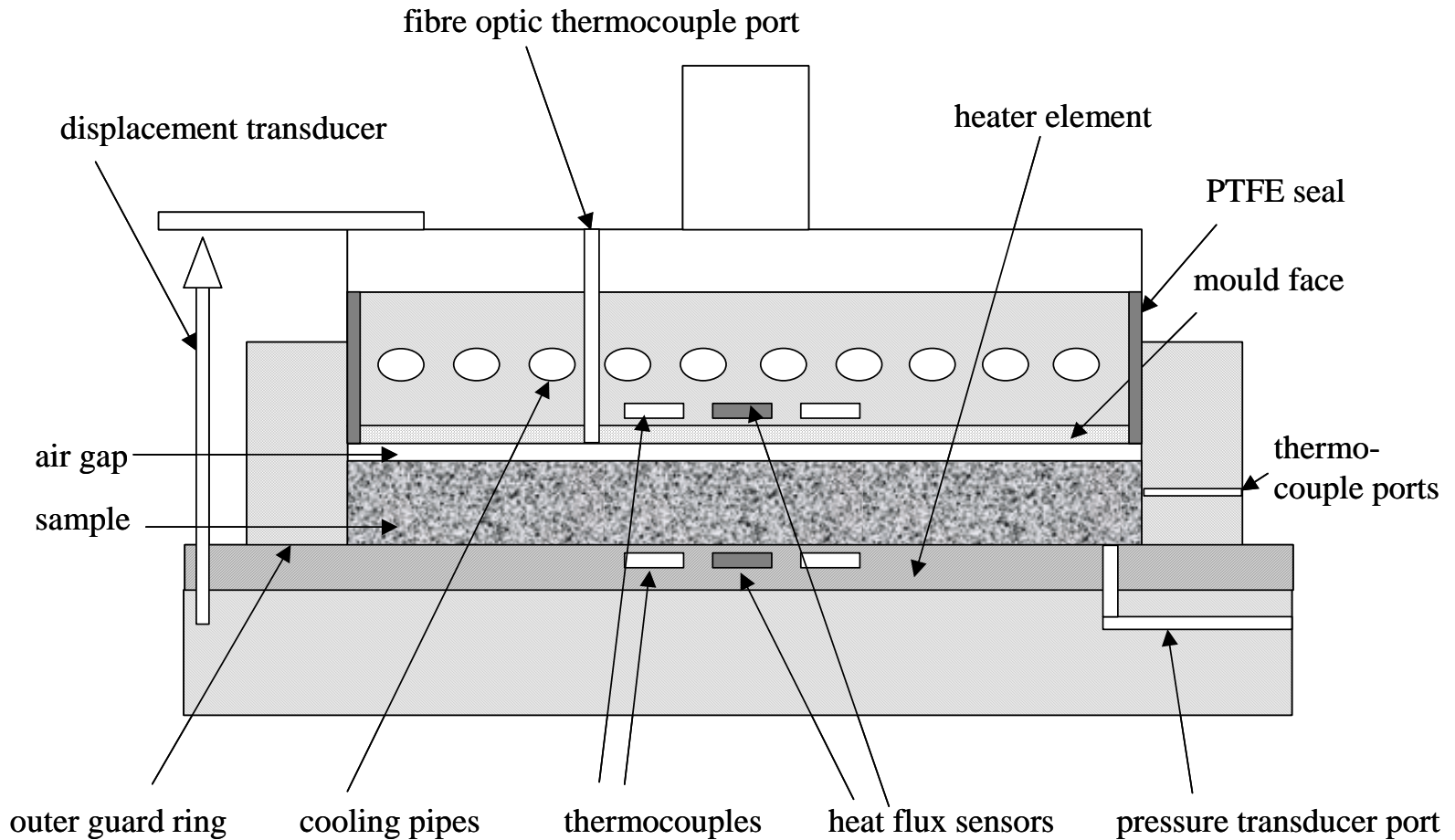


# Heat transfer apparatus

Side view



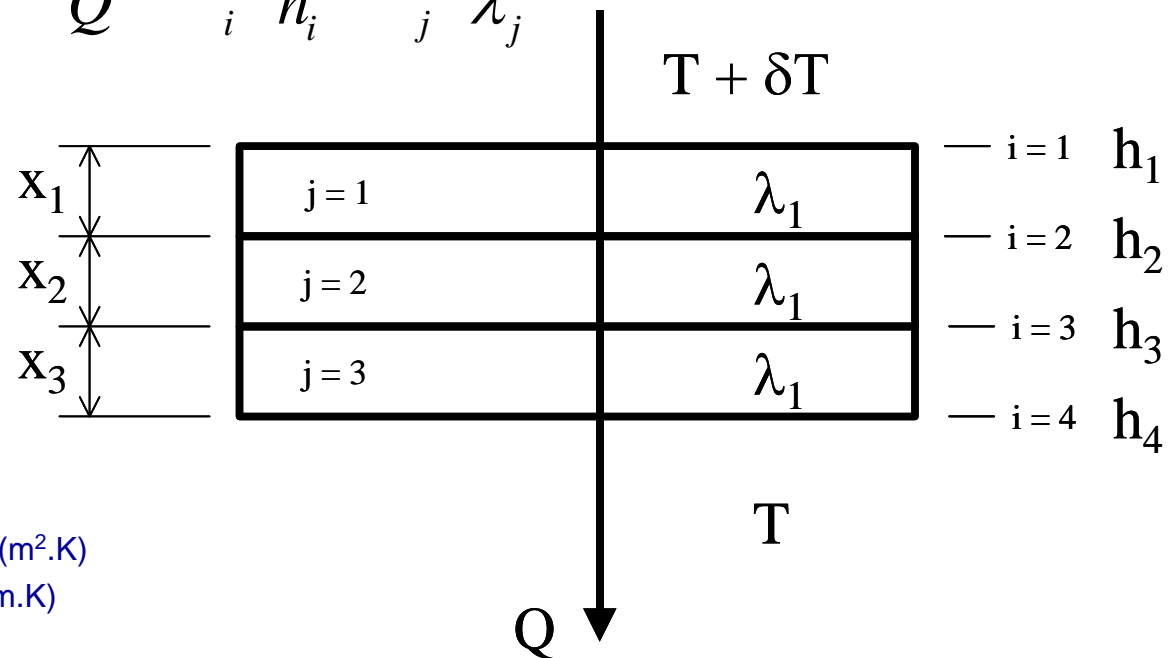
# Heat transfer apparatus



# Heat transfer: thermal resistance model

When materials are placed in series, their *thermal resistances*  $R_i$  ( $m^2K/W$ ) are added

$$R = \frac{\delta T}{Q} = \sum_i \frac{1}{h_i} + \sum_j \frac{x_j}{\lambda_j}$$

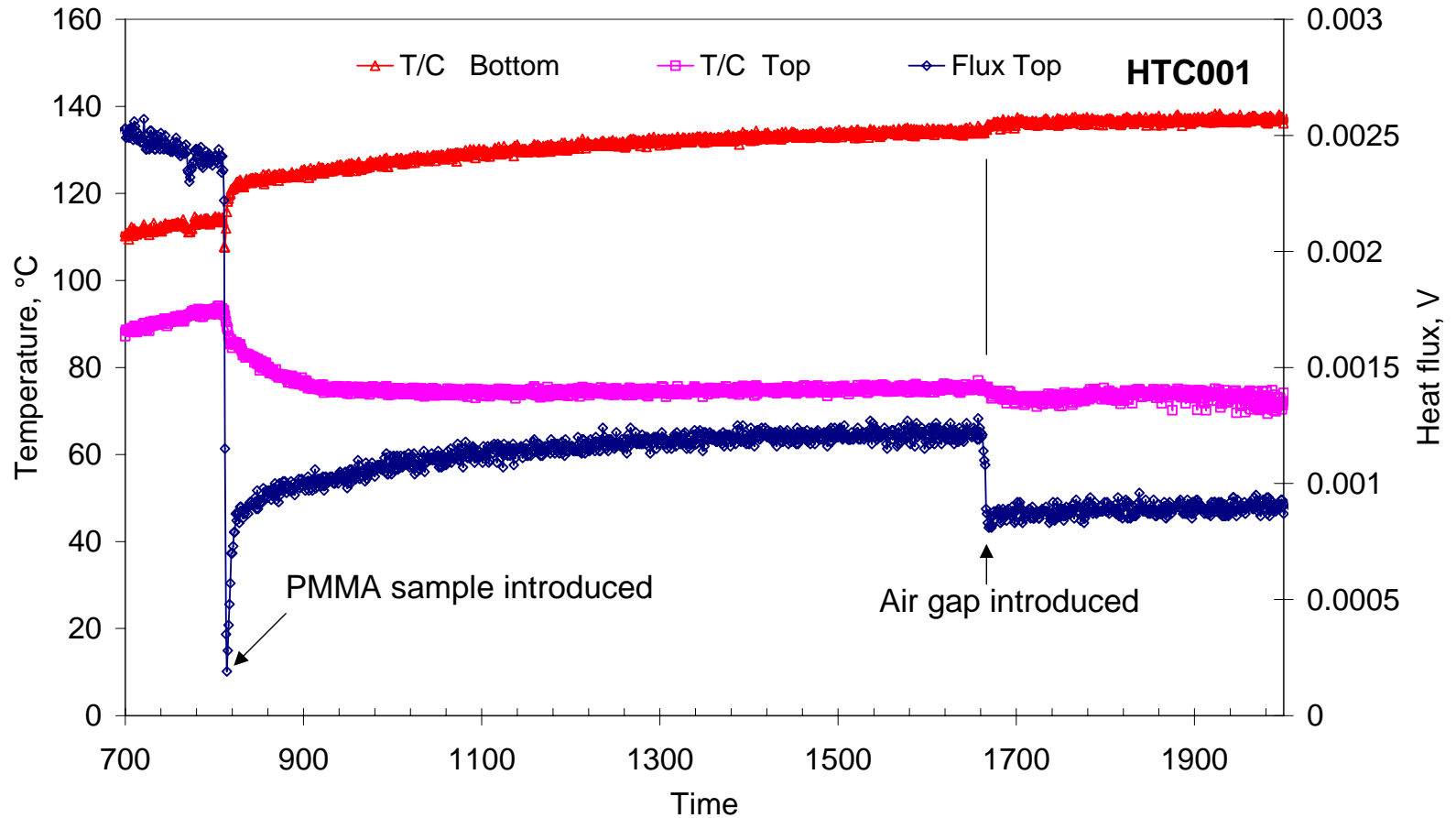


$h$  – heat transfer coefficient,  $W/(m^2.K)$

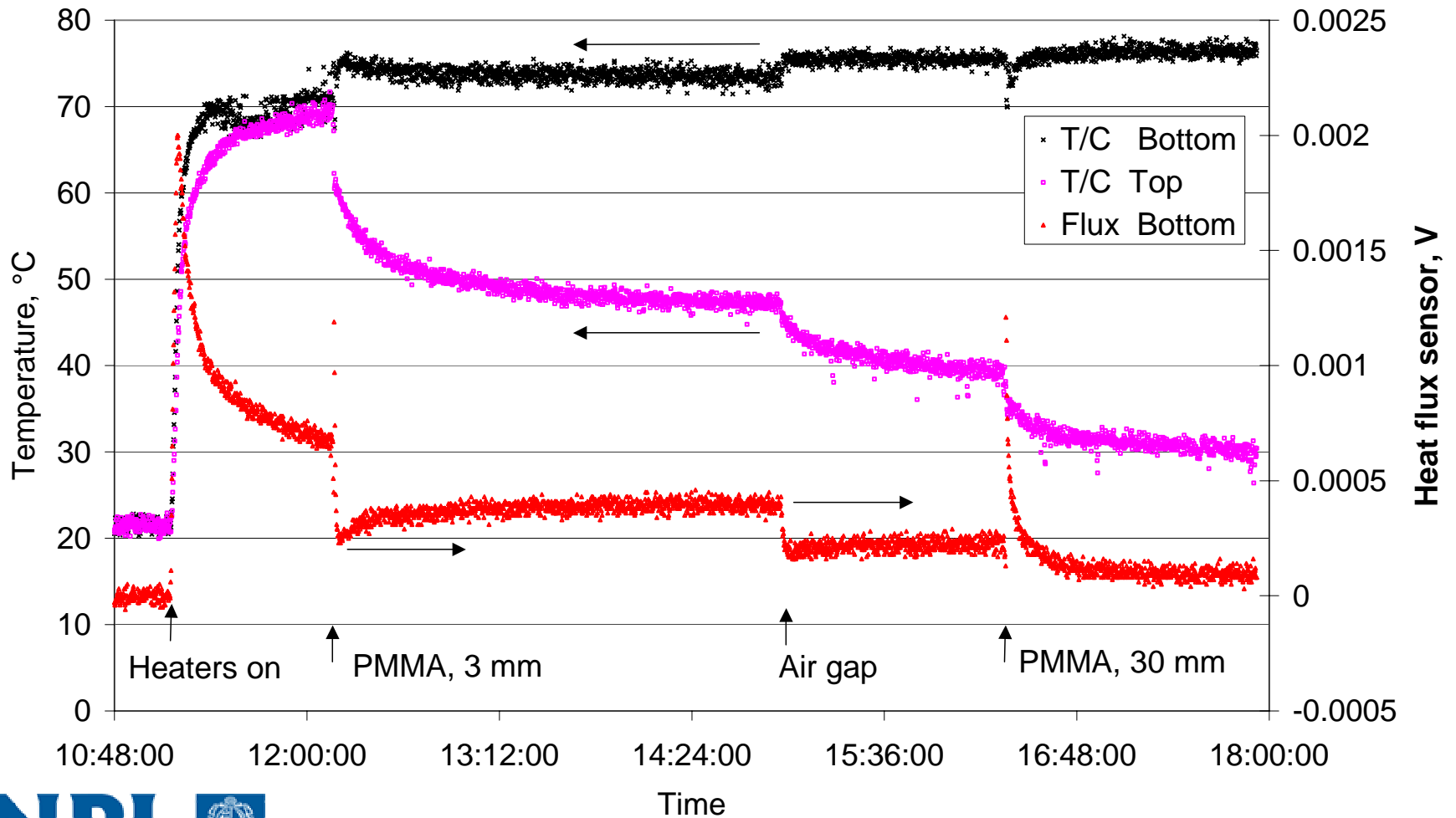
$\lambda$  – thermal conductivity,  $W/(m.K)$

$x$  – thickness, m

# Heat transfer



# Heat transfer

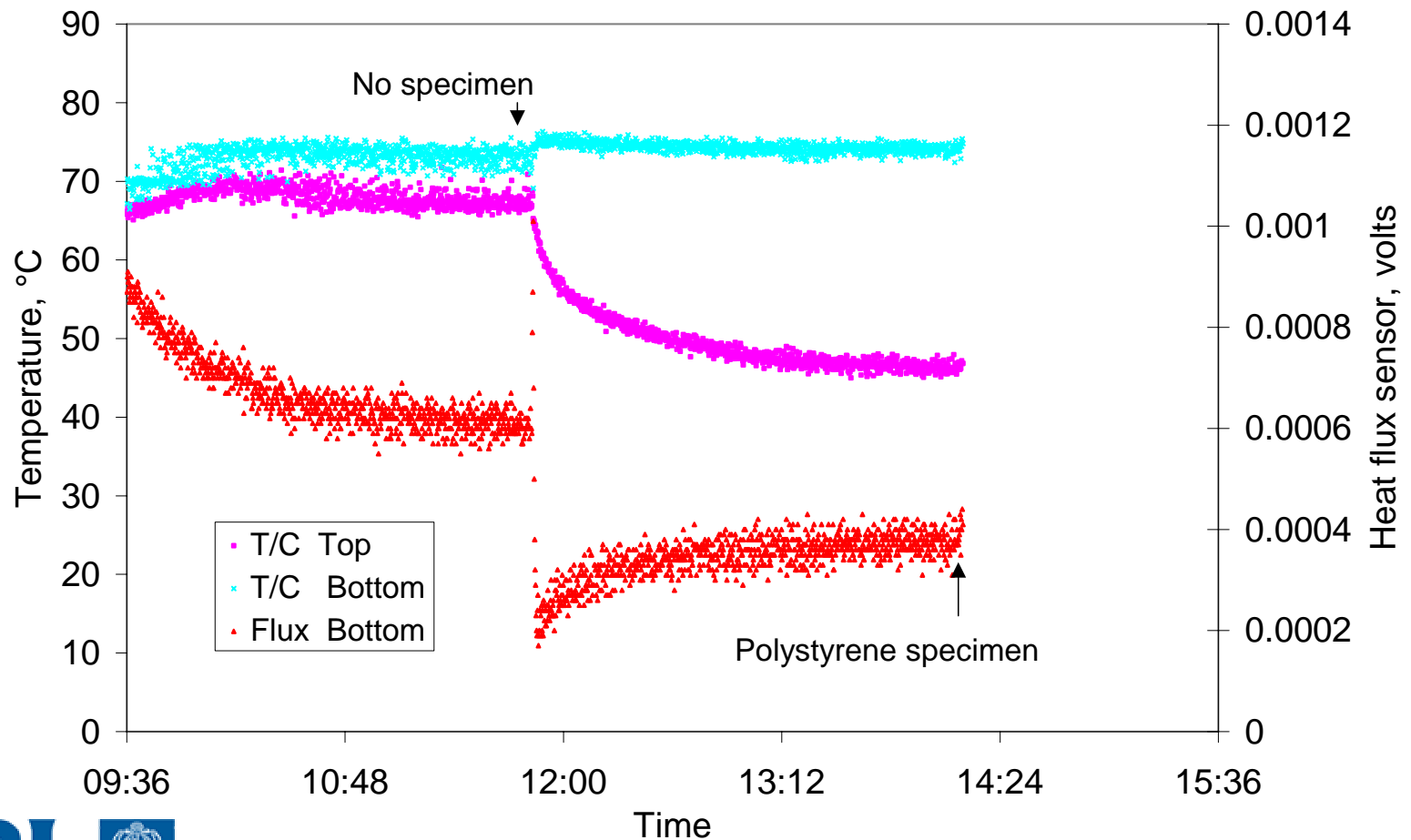


# Thermal conductivity measurement

Polystyrene

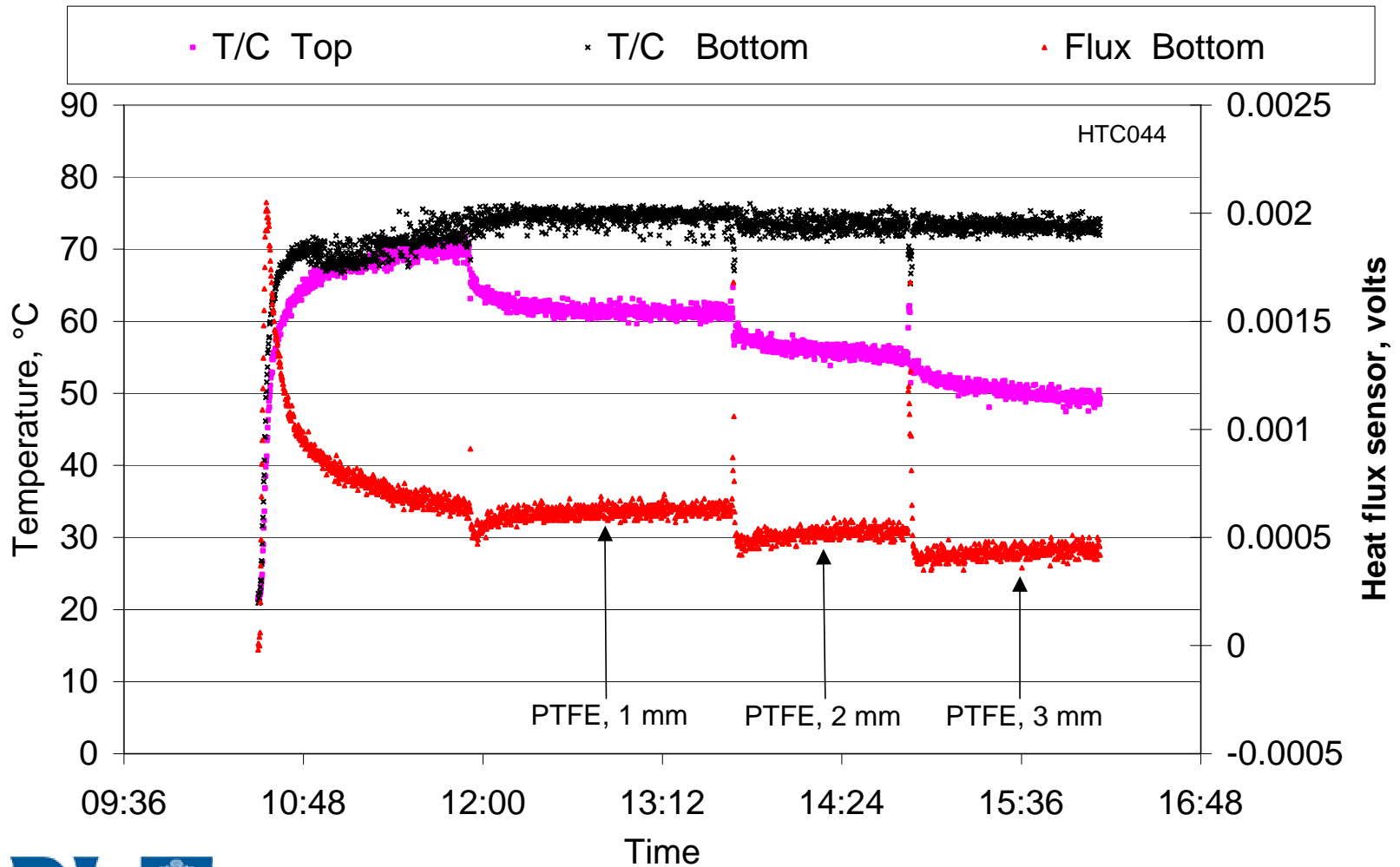
Line source method = 0.185 W/(m.K) at 20 MPa & 70 °C

Heat transfer equipment derived value = 0.170 W/(m.K)



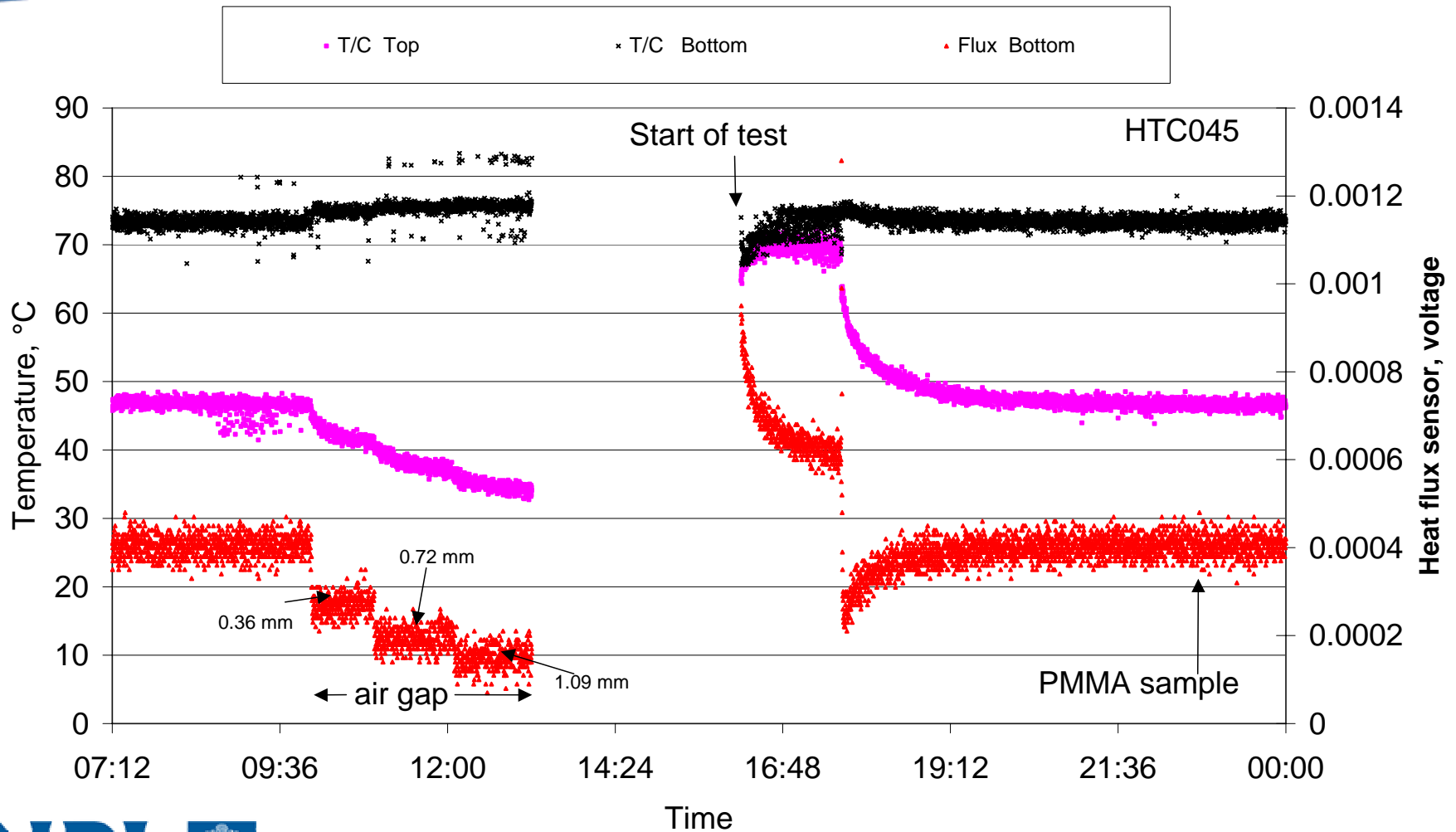
# Heat transfer coefficient: effect of specimen thickness

Specimen thickness, mm	1.03	2.15	3.02
Thermal conductivity, W/(m <sup>2</sup> .K)	0.25	0.28	0.27



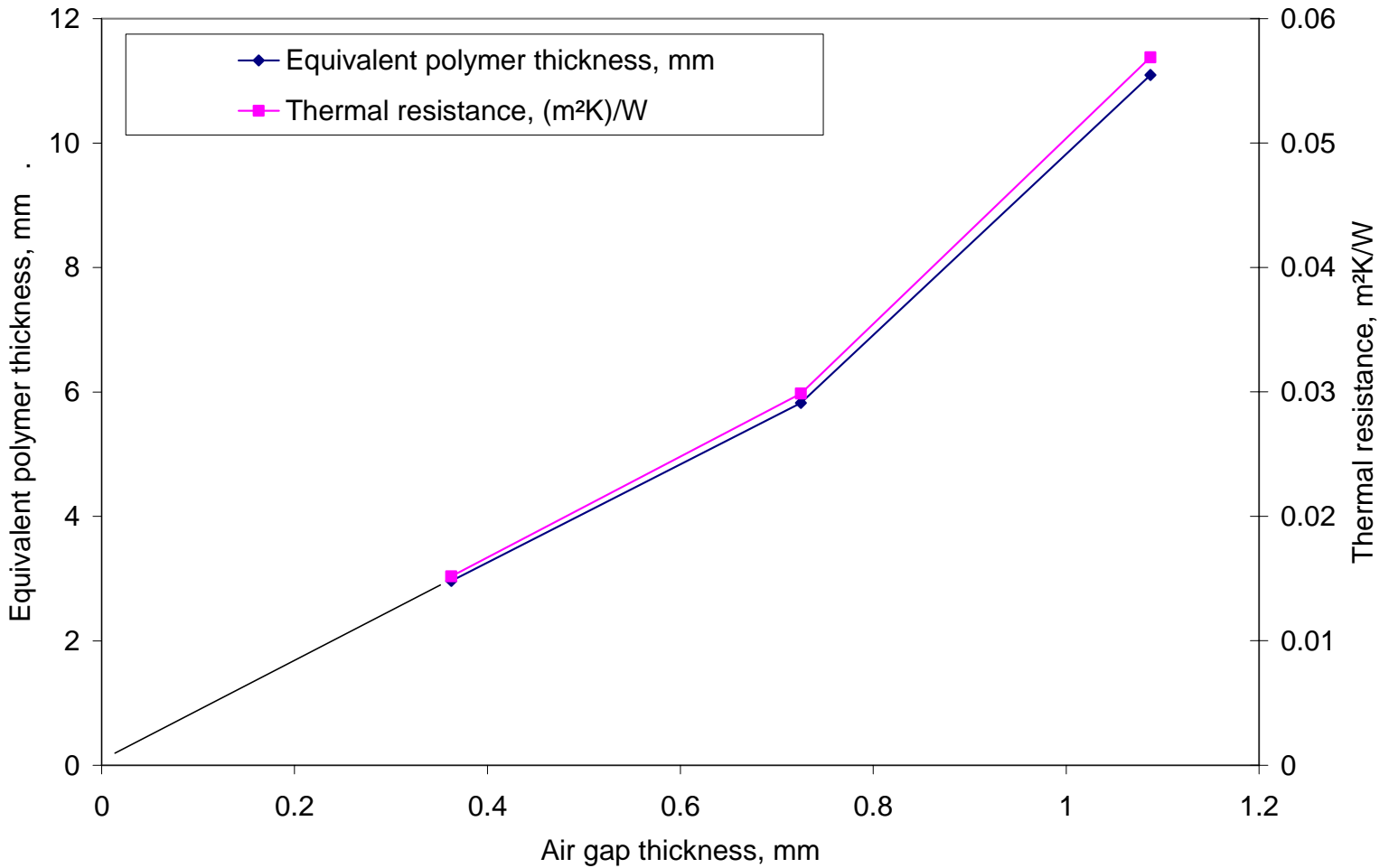
# Heat transfer coefficient: effect of air gaps

Air gap, mm	0.363	0.725	1.088
Equivalent polymer thickness, mm	3.0	5.8	11.1
Thermal resistance, (m <sup>2</sup> K)/W	0.015	0.030	0.057





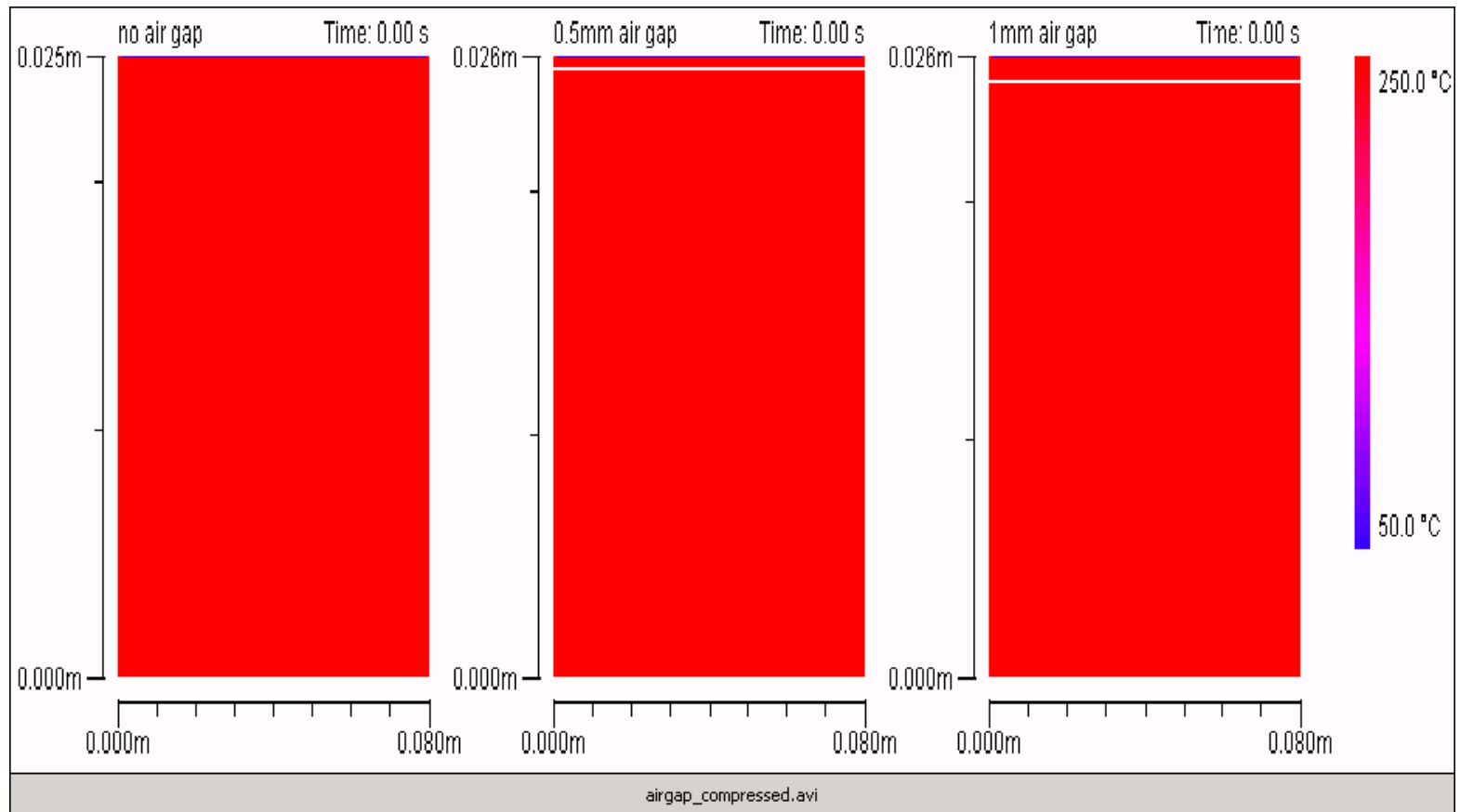
# Heat transfer coefficient: effect of air gap



- Effect of an air gap
- Effect of vertical thermocouple on distort the temperature field

# Air Gap

Mould at 50 °C with air gap of 0, 0.5 & 1 mm



# Heat Transfer Equipment Summary

- Measurements of thermal conductivity of polymers yielding reasonable values. However, need to
  - address signal noise and improve data analysis procedure
  - further validate instrument through thermal conductivity measurements
- Effect of air gap on thermal resistance quantified



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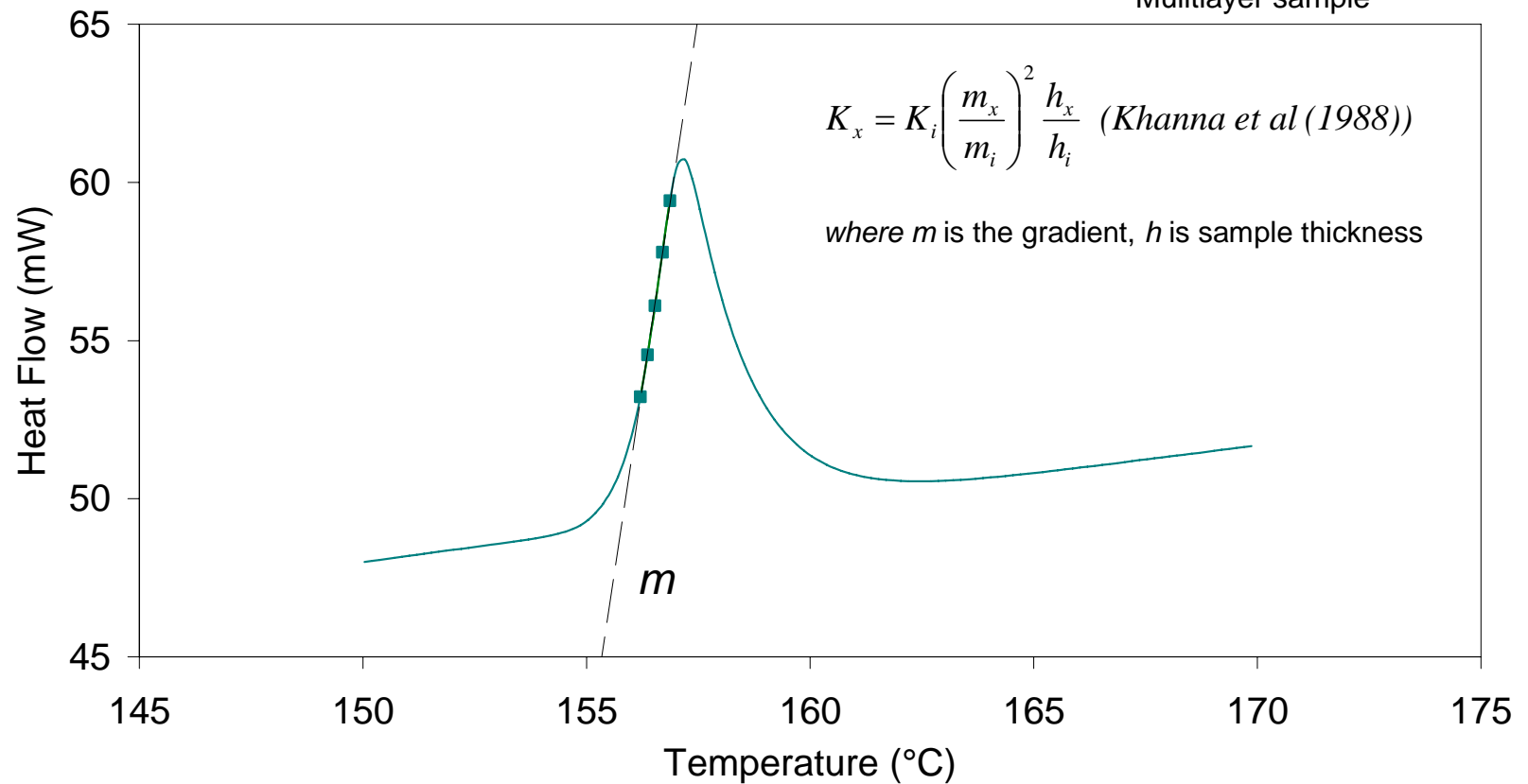
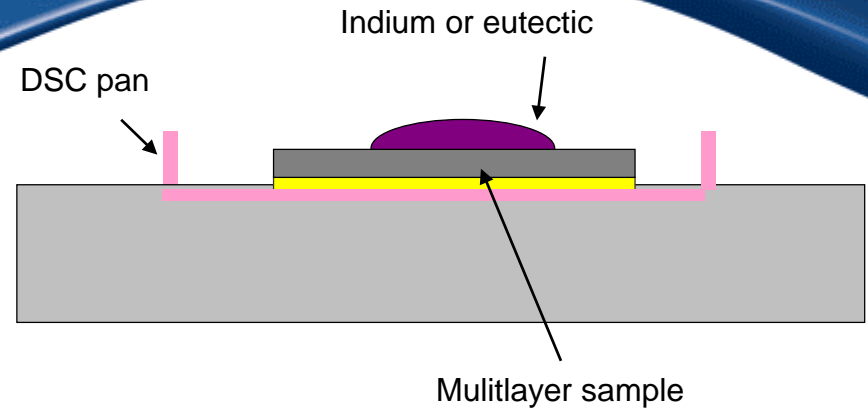
# INDUSTRIAL TRIALS Corus & Zotefoams

**Aim** is to investigate DSC method and demonstrate practical benefits of heat transfer measurements and modelling

- Corus
  - Thermal conductivity of plastisol coated steel before and after solidification
- Zotefoams
  - Heat transfer during cooling of polyolefin foam

- Use DSC method to measure thermal conductivity of bilayer Plastisol/steel
- Measure before and after solidification
- Data useful in predicting optimum line speeds
  - Earlier work had shown that the polymer layer was significant in terms of heat transfer

# DSC method for thermal conductivity





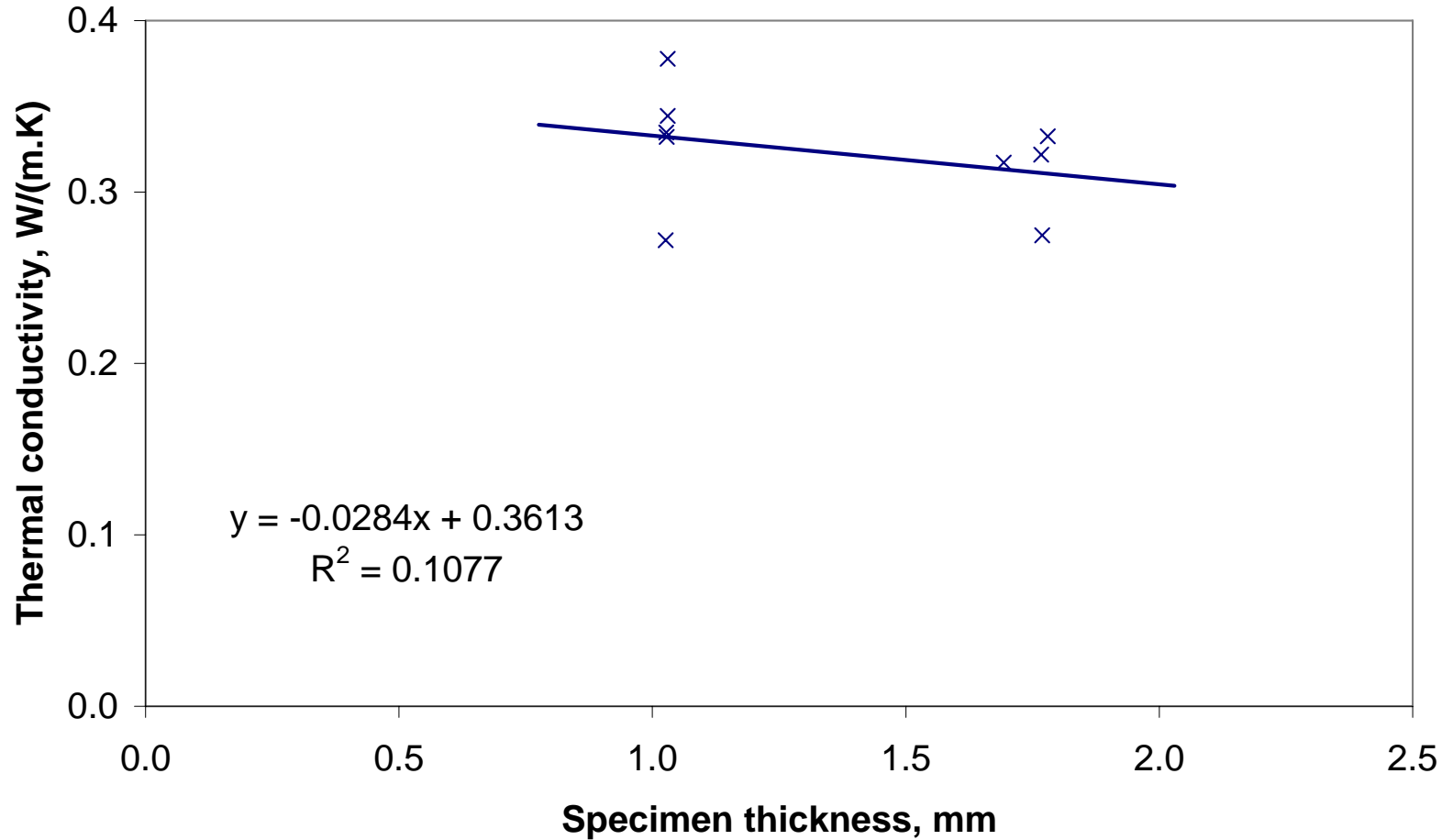
# DSC method for thermal conductivity

TEST ID	Specimen ID	Specimen gradient mW/°C	Specimen thickness mm	Thermal conductivity value - literature W/mK	Measured thermal conductivity* W/mK	Error
DSC098	PTFE + Indium	2.11	1.026	0.25	0.27	9%
DSC089	PTFE + Indium	2.34	1.027	0.25	0.33	34%
DSC087	PTFE + Indium	2.48	1.030	0.25	0.38	51%
DSC088	PTFE + Indium	2.37	1.030	0.25	0.34	38%
average 95% confidence §	PTFE + Indium	2.32	1.03	0.25	<b>0.33</b> <b>0.09</b>	33%
DSC092	PTFE + Indium	1.77	1.693	0.25	0.32	27%
DSC090	PTFE + Indium	1.75	1.767	0.25	0.32	29%
DSC099	PTFE + Indium	1.61	1.769	0.25	0.27	10%
DSC091	PTFE + Indium	1.77	1.780	0.25	0.33	33%
average 95% confidence §	PTFE + Indium	1.73	1.75	0.25	0.31 <b>0.05</b>	25%
DSC093	ref. PMMA + Indium	1.60	1.208	0.18	0.18	3%
DSC110	ref. PMMA + Indium	1.64	1.208	0.18	0.19	7%
DSC111	ref. PMMA + Indium	1.51	1.208	0.18	0.16	-9%
average 95% confidence §	PMMA + Indium	1.58	1.21	0.18	0.18 <b>0.01</b>	1%

\*Calculated assuming thermal conductivity of 0.18 W/(mK) for PMMA reference sample

§ 95% confidence = 2 x standard deviation

# DSC method for thermal conductivity

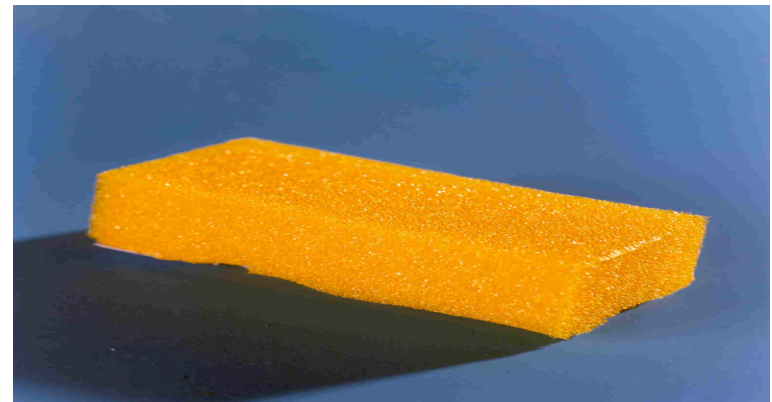


# DSC method for thermal conductivity

- Essential to use reference specimen of similar thermal conductivity as specimen to be measured
  - Repeatability 95% confidence levels up to approximately 25%
- Essential to carry out several repeat tests to improve on statistical significance of data
  - Not appropriate for testing molten/liquid samples (e.g. plastisols) – having constant and known sample thickness

Problem: waviness in foams – thermal issue

- Model heat transfer
- Measure (T, heat flux) over time
- Measure shrinkage
- Use to predict curvature

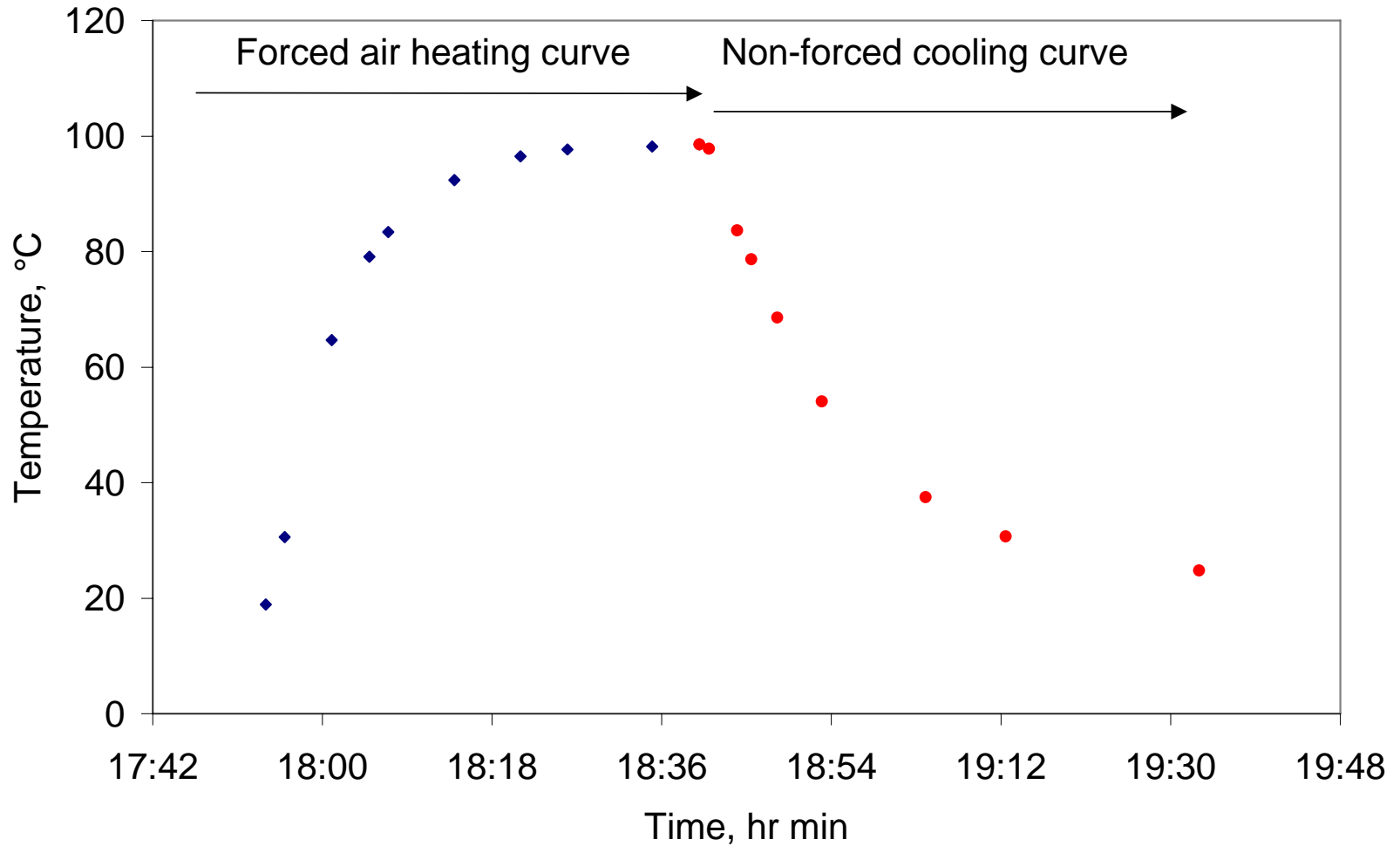


# Foams

Problem: waviness in foams – thermal issue



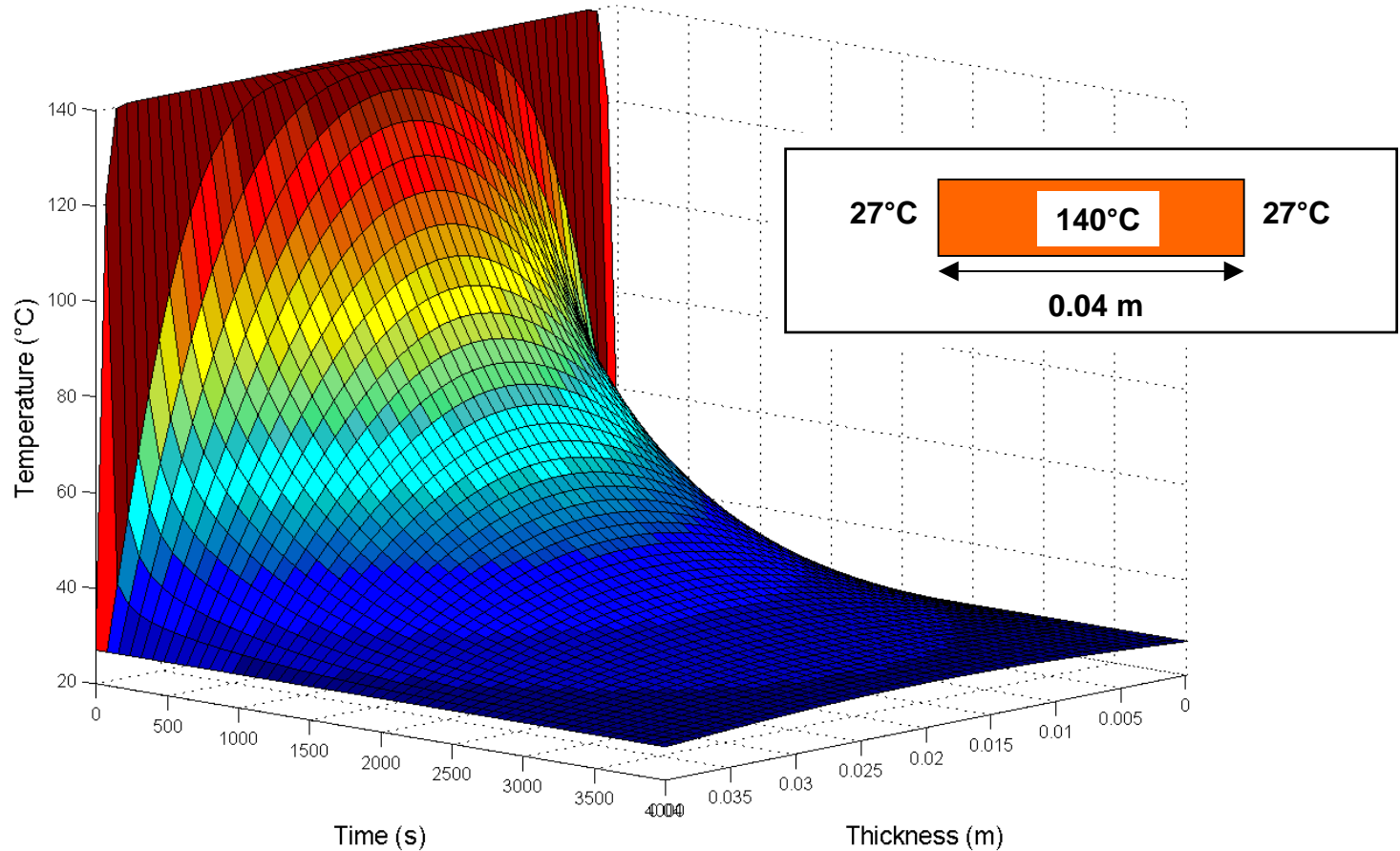
# Heating & cooling of foam block



# Numerical modelling of cooling of foam block

$\lambda = 0.004 \text{ W/m.K}$   
 $\rho = 16 \text{ kg/m}^3$   
 $C_p = 1555 \text{ J/kg.K}$

Transient 1D Solution



## **Initial observations and results suggest:**

- uneven cooling of foam sheet
- resulting in variation in shrinkage with position
- causing waviness of sheets

**Industrial trial to be performed 20 – 21 October 2005**

**Numerical modelling trials ongoing**



# **Standards for Thermal Properties Measurement of Plastics**

### ISO 11357 Plastics - Differential scanning calorimetry (DSC)

- ◆ ISO 11357-1: 1997 Part 1: General principles (being revised)
- ◆ ISO 11357-2: 1999 Part 2: Determination of glass transition temperature
- ◆ ISO 11357-3: 1999 Part 3: Determination of temperature and enthalpy of melting and crystallization
- ◆ ISO 11357-4: 2005 Part 4: Determination of specific heat capacity
- ◆ ISO 11357-5: 1999 Part 5: Determination of characteristic reaction-curve temperatures and times, enthalpy of reaction and degree of conversion
- ◆ ISO 11357-6: 2002 Part 6: Determination of oxidation induction time
- ◆ ISO 11357-7: 2002 Part 7: Determination of crystallization kinetics

### **ISO 22007 Plastics –**

#### **Determination of thermal conductivity and thermal diffusivity**

ISO/NWIP 22007-1 Part 1: General principles

ISO/CD 22007-2 Part 2: Transient plane source hot-disc method  
(Gustafsson)

ISO/CD 22007-3 Part 3: Temperature wave analysis method

ISO/CD 22007-4 Part 4: Laser flash method

## Proposal to develop Line Source Method for Thermal Conductivity as part of ISO 22007 series

### Method currently standardized as:

- ASTM D 5930-01, Test Method for Thermal Conductivity of Plastics by Means of a Transient Line-Source Technique

However this does not make provision for:

- effect of applying pressure to minimize measurement scatter, and
- effect of pressure on thermal conductivity

**ISO TC61 SC5 WG8 Thermal Properties.**

## Proposed intercomparison of thermal conductivity methods

To be carried out, in support of standardisation activity, including at least:

- ◆ Transient plane source hot-disc method (Gustafsson)
- ◆ Temperature wave analysis method
- ◆ Laser flash method
- ◆ Line source probe

To be led by NPL

# Summary – Heat Transfer

- Heat transfer coefficient apparatus now being used
  - Design assisted by numerical modelling studies
  - Effect of uncertainties investigated (report available)
- Melt thermal conductivity measurements
  - Nano-filled materials
  - Powders/granules
  - Effect of pressure
  - Effect of uncertainties investigated (report available)
- ISO Standards being developed
- New IAG members facility on website  
<http://www.npl.co.uk/materials/polyproc>

# The next 6 months

- Complete commissioning trials on heat transfer coefficient equipment
- Complete industrial demonstrations (Corus & Zotefoams)
- Dissemination of thermal conductivity and heat transfer coefficient measurement work



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# Heat Transfer Project 2005-08



## H1: Measurement methods for heat transfer properties data for application to polymers

### Objectives:

- Development of the method for the measurement of heat transfer properties across surfaces (particular interest has been expressed in the effect of the solid/air interface)
- Industrial case study to demonstrate the value of reliable heat transfer data
- Support development of standards for measurement of thermal properties of plastics, including an intercomparison of thermal conductivity methods that are being proposed for standardisation
- Assessment of uncertainties in heat transfer data and effect on modelling predictions
- Development of a new user-friendly web-enabled modelling facility, to facilitate industrial adoption of the above

# Heat Transfer Coefficient - future activity

- Investigate effect of:
  - Air gap between polymer & top plate (simulating shrinkage and sink marks) (Cinpres) and compare with numerical modelling predictions
  - Different surface finishes/mould materials (RAPRA)
  - Effect of mould release agents

## Potential areas of relevance for future work to increase understanding of heat transfer:

- Effect of air gaps (EGM)
- Effect of mould materials (RAPRA)
- Gas assisted injection moulding (GAIM)
- Water assisted injection moulding (WAIM)
- Additives, fillers – e.g. effect of nano-particles on thermal conductivity
- Micro-moulding

## Potential areas of relevance for future work to increase understanding of heat transfer:

- Effect of nano-particles on heat transfer in polymers
- Effect of dispersion of nano-particles on heat transfer
- Measurement of heat transfer within micro-fluidic systems
- Developing techniques for measuring heat transfer properties of foams
- Curing of fibre/matrix composites and cross-linking of rubbers

## **Your:**

Ideas,  
comments,  
suggestions,  
participation,  
contributions, ...

to steer the project to maximise  
the benefits to you.



**Any other business**

**Tea & coffee available**