

Where DSP meets Measurement Science: A Sound Example

By Andrew Hurrell PhD

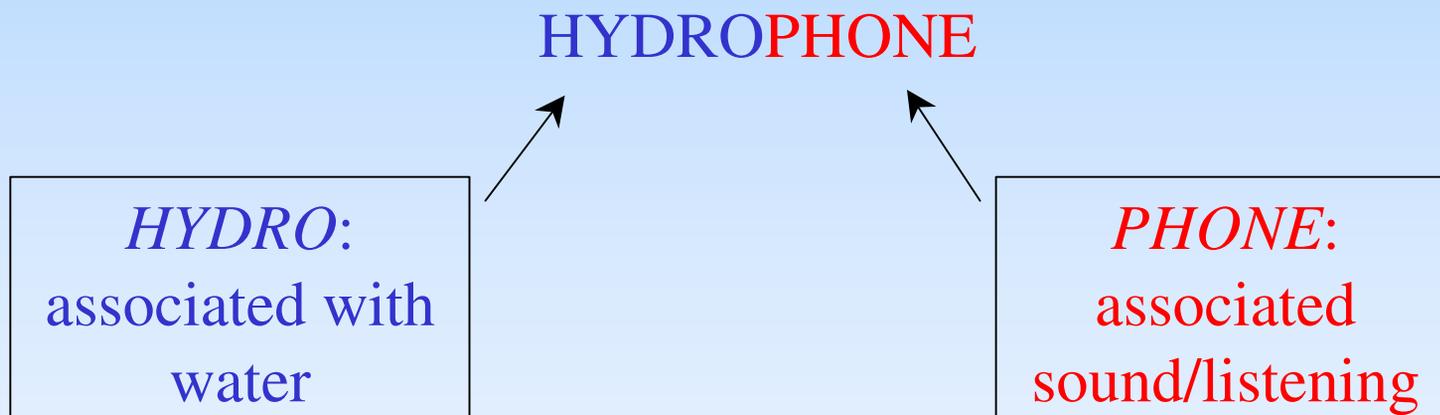
Measuring ultrasound – why bother?

- 6 million ultrasound scans within NHS during 2004-2005
- Ultrasound has potential for:
 - Thermal damage: enough to “cook” tissue as a form of cancer therapy
 - Mechanical damage: Many cleaning baths use ultrasonic sterilisation
- YET, ultrasound is one of the safest imaging modalities
 - Because it is non-ionising, but also VERY WELL REGULATED
 - UK is the world leader in ultrasound standards



Ultrasonic metrology: getting started

- Most ultrasonic pressure measurements use hydrophones



Common hydrophone types



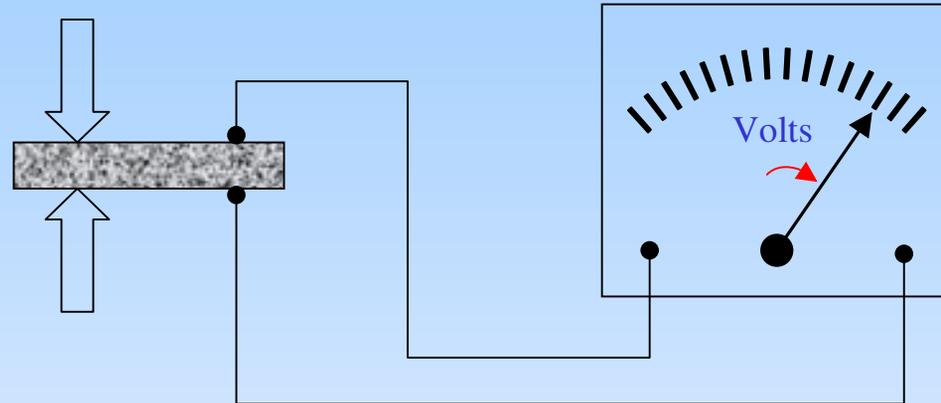
Membrane



Needle/Probe

Principles of hydrophone operation

- Most hydrophones use piezo-electric materials.
 - piezo – from Greek meaning “to press”.
- Applied pressure produces a voltage



BUT, we want to measure pressure not voltage

THEREFORE we require a means of deriving pressure waveforms from the voltages that have been measured

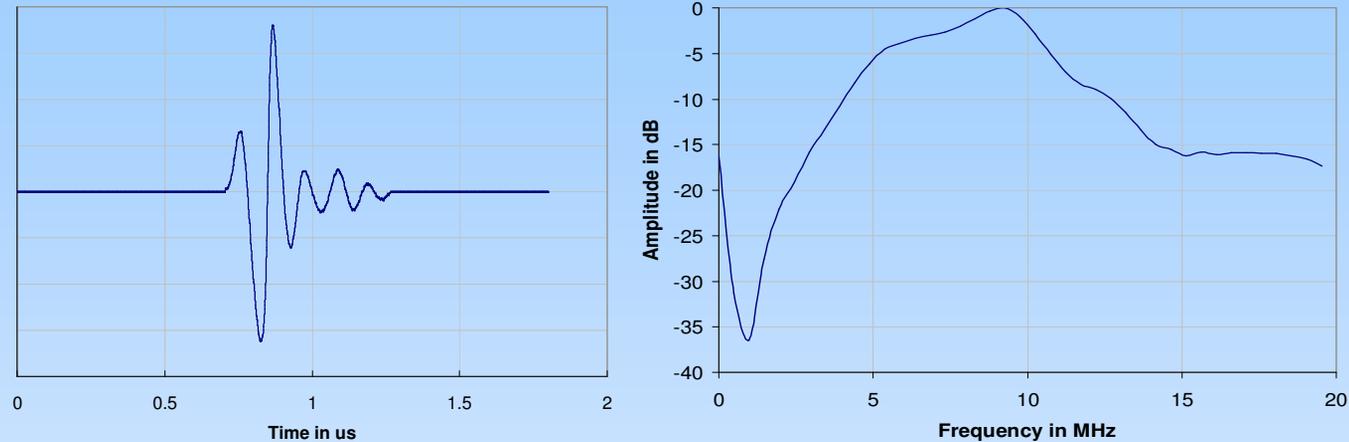
The hunt for a pressure waveform

- Calibration
 - Any given hydrophone needs calibration (preferably by an accredited lab such as NPL) to derive the relationship between output voltage and measured pressure
 - Calibration figure (hydrophone sensitivity) is often frequency dependant
- Measurement
 - Hydrophone sensitivity applied to measured waveform to provide true pressure waveform

Calibration – requirements

- Ultrasonic hydrophones operate over wide frequency range. For example
 - Lower frequency: 100 kHz to 10 MHz
 - Higher frequency: 1 MHz to 60 MHz
- Need ultrasound source capable of covering this wide range

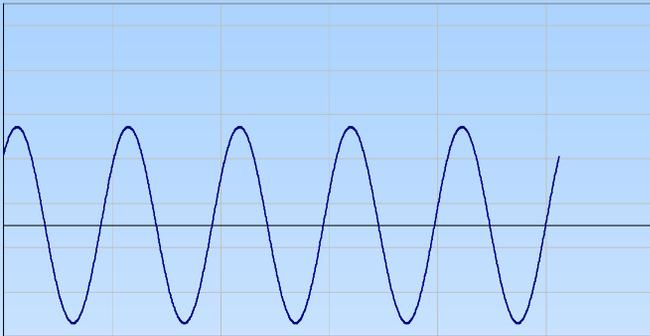
Calibration – sources



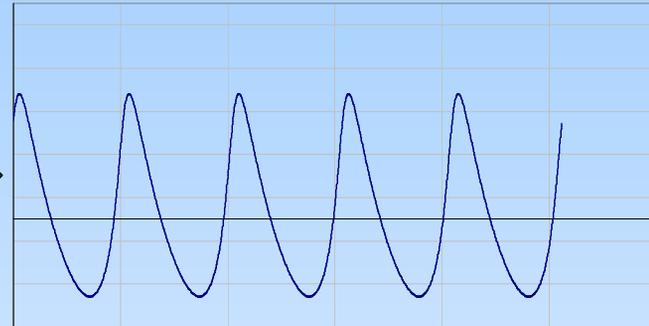
- Sources of ultrasound often have limited bandwidth (<100% of centre frequency)
 - e.g. 0.5-1.5MHz (centre 1 MHz), 5-15 MHz (centre 10 MHz)
 - Many sources required to cover required range
 - Multiple setup/alignments are VERY time consuming

Calibration – nonlinear propagation

Completely Linear



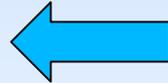
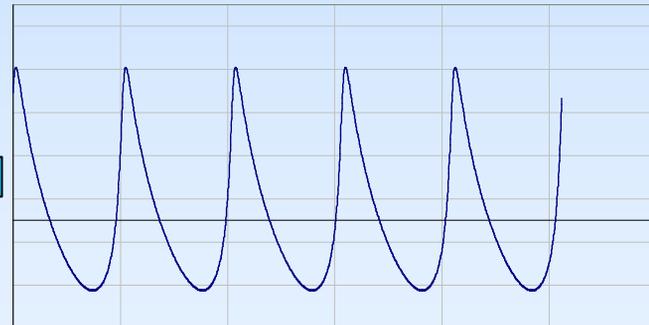
Notable Asymmetry



Well Developed Shock Front

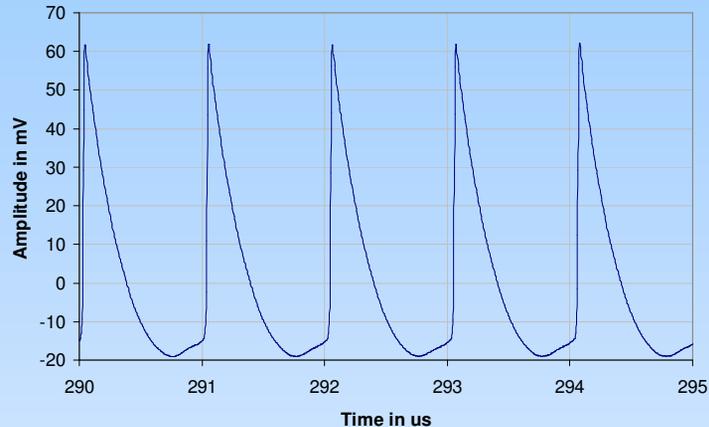


Shock Front Starting

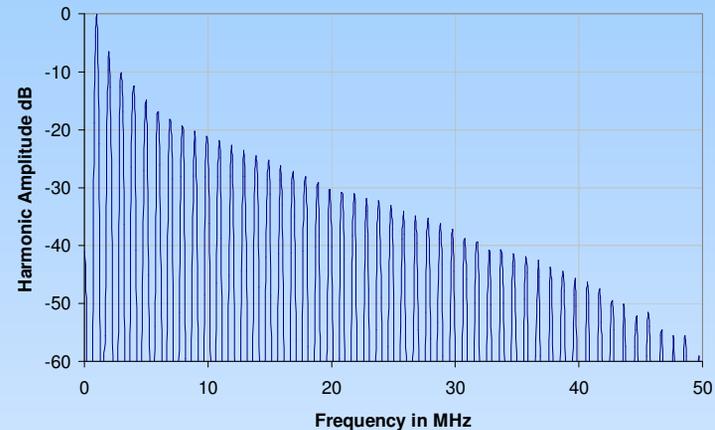


Calibration – shockwave behaviour

Experimental Shock Wave



Experimental Shock Wave Spectrum



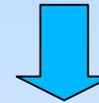
- Nonlinear propagation has “pumped” energy into harmonics at integer multiples of fundamental
- Spectral amplitudes can be obtained via FFT of temporal waveform

Calibration – process overview

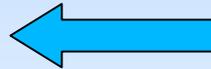
Measure ultrasonic field with device under test



Remove test device and replace with reference hydrophone*



Measure ultrasonic field with reference hydrophone



Compare spectra from two hydrophones to obtain calibration figure for test device

* Reference hydrophone's calibration will have been determined by other methods and often against (inter)national primary standards

Calibration – pitfalls for the unwary

- Accuracy of calibration is dependent on determination of spectral amplitude at each frequency
- Therefore must carefully consider
 - Signal Bandwidth relative to Sampling Frequency
 - Signal Periodicity and Windowing

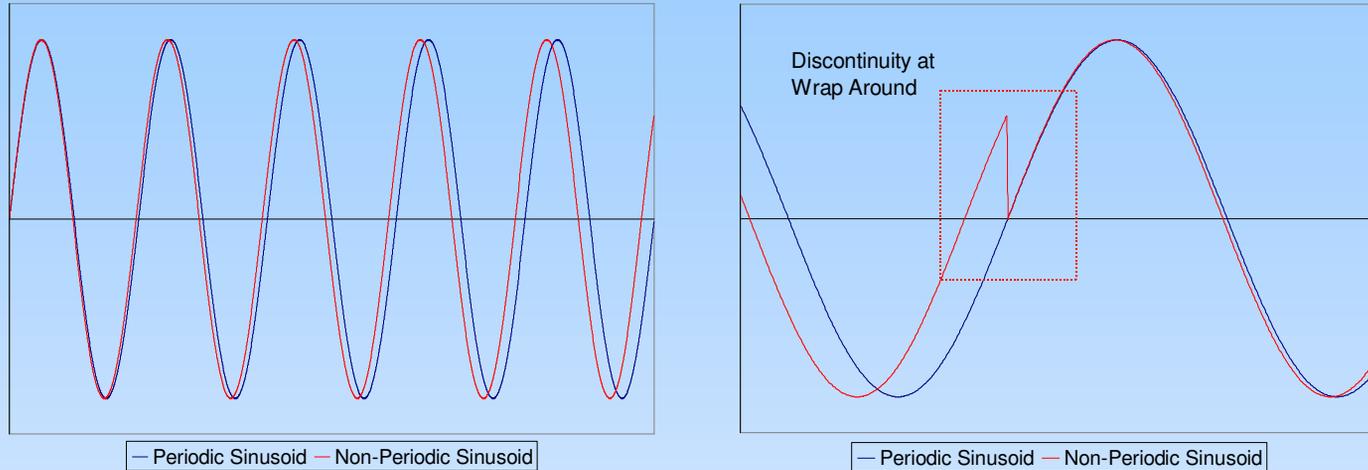
Calibration – pitfalls – bandwidth

- Sampling frequency of digitise waveforms should satisfy Nyquist-Shannon criteria
 - 100th Harmonic easily generated with shocked waves
 - If fundamental = 2 MHz, highest harmonic ≥ 200 MHz
 - Sampling frequency should be at least 400 MHz, preferably much higher (≥ 1 GHz)

OR

- Low-Pass filtered so that $2 * f_{\max} < f_{\text{sampling}}$
- Inadequately sampled signal will suffer from aliasing causing significant amplitude errors

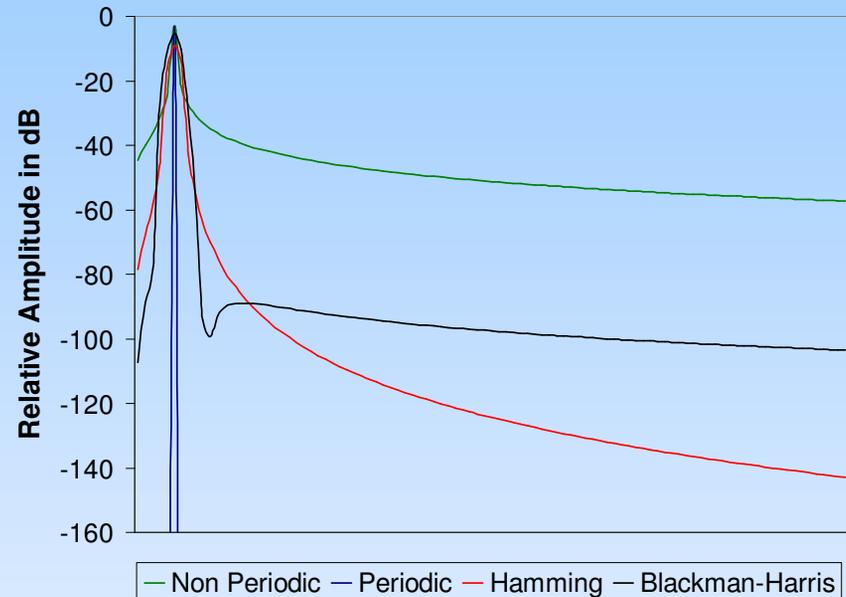
Calibration – pitfalls – periodicity



- Fast Fourier Transform methods implicitly assume that input signals are periodic
 - only true if the sampled data set contains a whole number of cycles
- Non Periodic signals have wraparound discontinuities
 - causes broadband spectral leakage

Calibration – pitfalls – windowing

- Window functions
 - Minimise spectral leakage at the expense of other factors, such as
 - Broader spectral peaks
 - Reduced amplitude of peaks



- Blackman-Harris window preserves amplitude well
 - Most important for this application

Calibration – summary

- A very broadband source is provided by non-linear propagation
- Calibration process reliant on accurate spectral amplitude measurement
 - Careful selection of window function
- Signal can have very wide bandwidths
 - High sample rate needed

Application of DSP principles and techniques are essential for accurate calibration

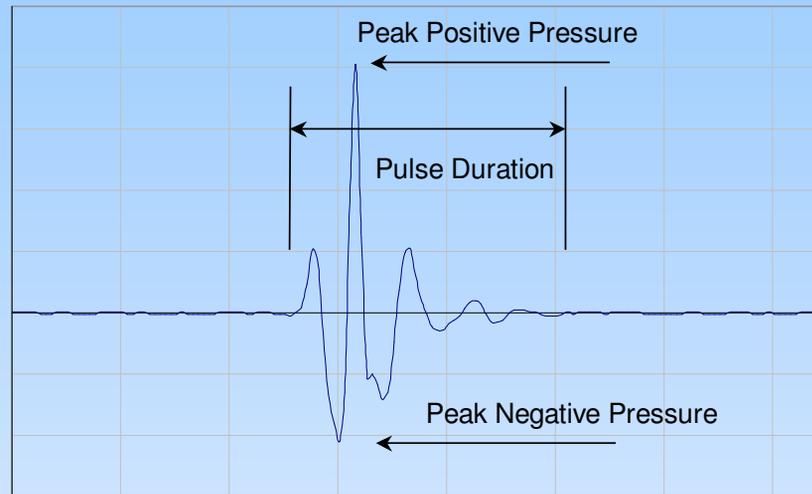
Measurement – process overview

voltage to pressure conversion

- Hydrophones calibration provides the conversion factor (hydrophone sensitivity) between voltage and pressure
- A hydrophone's sensitivity varies as a function of frequency and may be a complex quantity (magnitude and phase)

How best should this calibration data be used?

Measurement – regulatory parameters



- International standards prescribe limits on many exposure parameters
- Pressure parameters
 - related to mechanical damage potential
 - often based on time domain waveform shape
- Intensity parameters
 - related to thermal damage potential

Measurement – the current approach

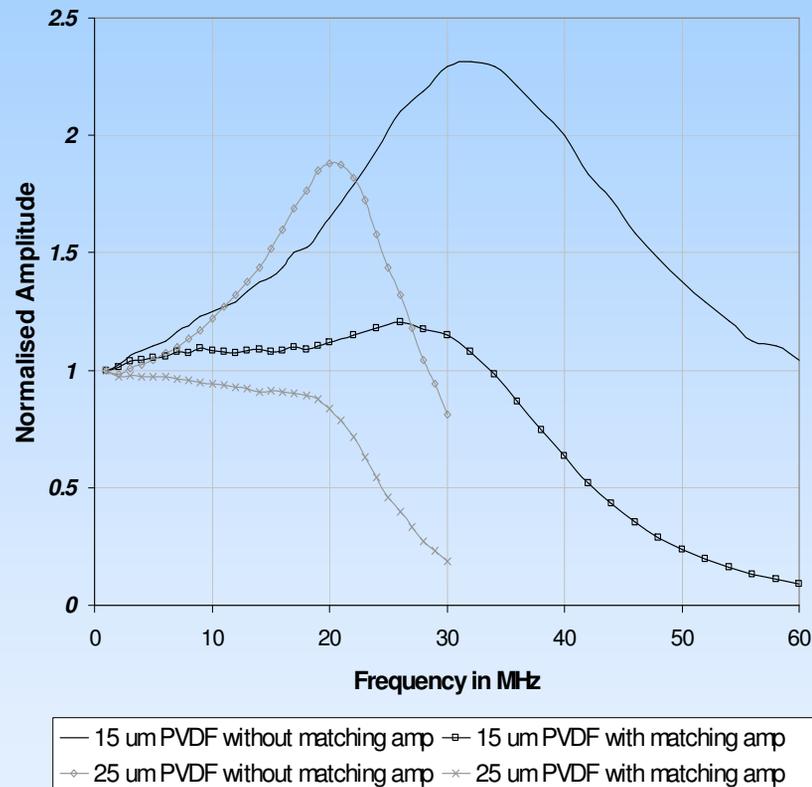
- Acoustic pressure is *approximated* from the measured voltage using the hydrophone sensitivity at the acoustic working frequency of the source

$$p(t) = \frac{v(t)}{M(f_{awf})}$$

- $v(t)$ is the measured hydrophone voltage
- $M(f_{awf})$ is the hydrophone sensitivity at the acoustic working frequency
- Only valid when hydrophone sensitivity has very little variation as a function of frequency
- Has no possibility to account for phase response

Measurement – distortion of reality to conform with existing standards

- Flattens frequency response up to thickness resonance frequency (f_r)
- Significantly attenuates beyond f_r
- Membrane hydrophones have inherent useable bandwidth at least 50% above f_r



Measurement – is bandwidth important ?

- Current diagnostic transducers often have centre frequencies in the range 10-15 MHz
- Current Standards require hydrophone bandwidth to extend to the minimum of :

FDA	5 times the centre frequency or 40 MHz
IEC	8 times the acoustic working frequency or 40 MHz

- Limited upper bandwidth will restrict the ability to resolve sharp peaks and may lead to poor determination of many intensity parameters

Measurement – is phase important ?

- Phase information will not affect the total energy in a signal but may significantly change the waveform shape.
 - Many acoustic parameters may be affected
- A hydrophone's phase variations should not be neglected if they occur well within the bandwidth of the source signal,
 - Membrane hydrophones only exhibit deviation from linear phase near f_r
 - Needle hydrophones show significant phase variations at lower frequencies

Measurement – hydrophone deconvolution

A better approach?

$$p(t) = \mathfrak{F}^{-1} \left\{ \frac{\mathfrak{F}\{v(t)\}}{M(f)} \right\}$$

- Where \mathfrak{F} and \mathfrak{F}^{-1} are the Fourier and inverse Fourier transforms and $M(f)$ is the hydrophone sensitivity as a function of frequency
- $M(f)$ can be a real (magnitude only) or complex (magnitude and phase) quantity

Measurement – the advantages of deconvolution

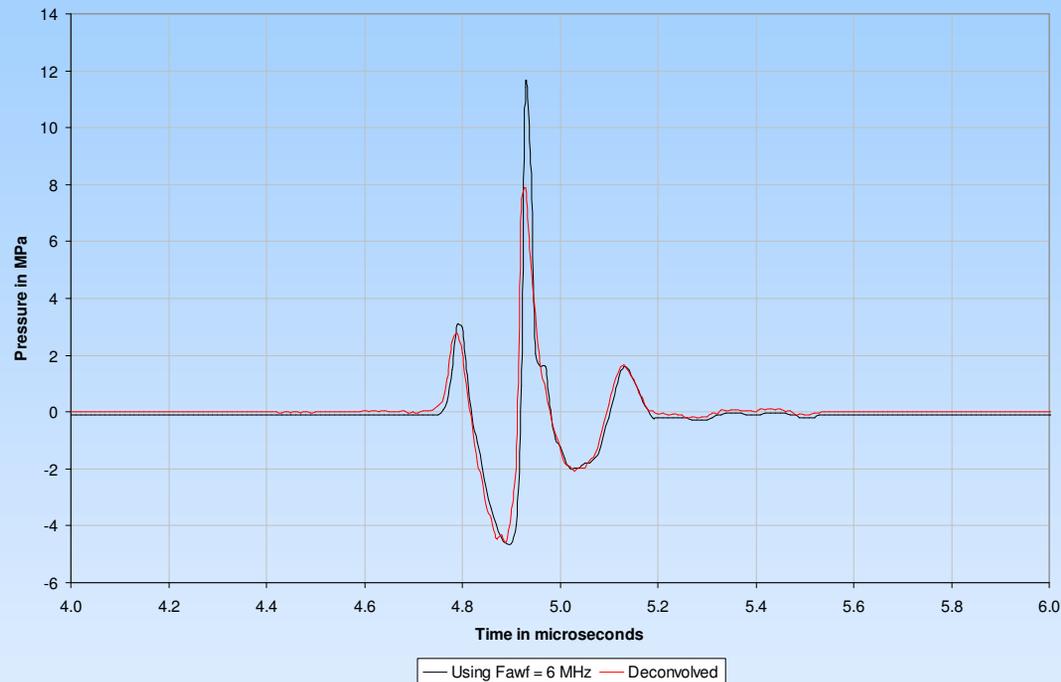
- Uses ALL available calibration data of the hydrophone
 - and is therefore a more accurate display of true acoustic pressure
- Can make use of phase data where available
- Real time display of acoustic pressure waveforms

Any other method of converting hydrophone voltage to pressure can only be a more crude approximation

Measurement – possible disadvantages?

- Hydrophone calibration data is only available at sparse frequency increment
 - Cubic spline interpolation easily and accurately overcomes this issue, and this can be precomputed for any given hydrophone
- Full characterisation of a diagnostic ultrasound machine may require thousands of measurements
- The additional computation will increase the measurement time
 - FFTs take a few milliseconds on modern PCs
 - If efficiently implemented, the deconvolution operation can be done during the time taken to move the hydrophone to its next location

Measurement example 1– output of ultrasonic scanner



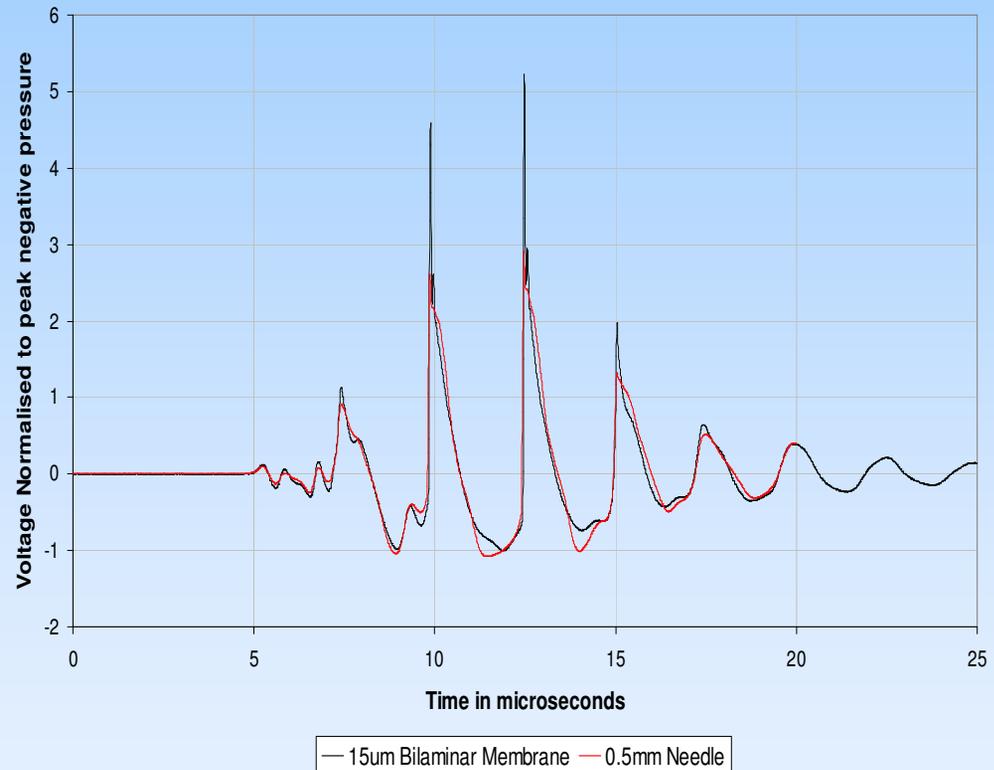
- Membrane overestimates energy at higher frequencies due to frequency response curve (NB $F_{awf} = 6$ MHz)

Measurement example 1– effect on exposure parameters

- Relative to deconvolution with magnitude and phase data, the single value method:
 - overestimated peak positive pressure by nearly 50%
 - underestimated peak negative pressure by 4%
 - NB a critical exposure parameter relies of peak negative pressure
 - overestimated intensity by nearly 20%

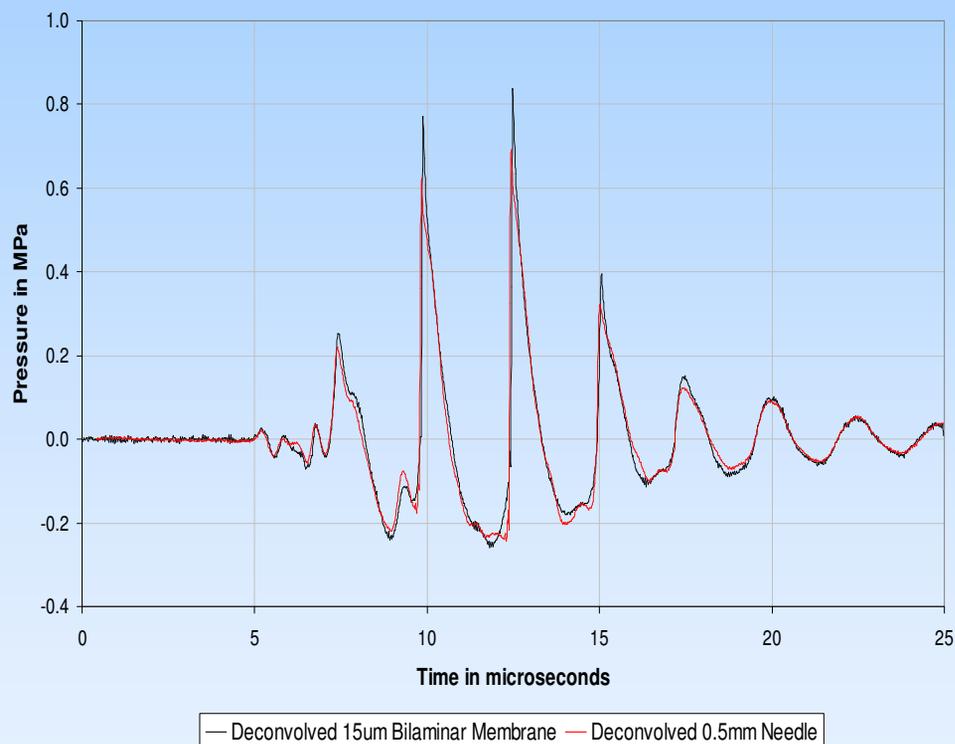
Measurement example 2 – needle hydrophones

- A broadband field was measured with
 - a membrane hydrophone
 - a deliberately non-flat (poor) frequency response needle hydrophone



Measurement example 2 – needle hydrophone deconvolution

- **Magnitude only** deconvolution used (phase data not yet available)
- Deconvolved waveform shows much better agreement with the membrane reference



Measurement example 2 – The effect on exposure parameters for needle hydrophones

- Using magnitude only deconvolution reduces:
 - Peak positive pressure error from 30% to 18%
 - Peak negative pressure error from 12% to 5%
 - Intensity error from 19% to 4%

Measurement – Summary

- Hydrophone deconvolution:
 - Makes use of ALL available calibration data
 - Dramatically reduces measurement error - even with **magnitude data only**
 - Can easily incorporate phase response data where available
 - Utilises modern DSP techniques as its core computation
- These developments have only become available with increased computational speed/power/storage

New hydrophone usage standards now incorporate hydrophone deconvolution techniques

Conclusions

- Ultrasound metrology inherently involves broadband signals
 - Mono-harmonic methods are inappropriate
- Most ultrasound data is acquired digitally and therefore DSP principles are essential for accurate measurements
- Application of FFT techniques is considerably reducing measurement errors

DSP – the only sensible way forward!