

Monte Carlo simulations for a prototype calorimeter for HDR brachytherapy sources

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Overview

- Motivation: Ionometry and calorimetry
- MC calculations for calorimeter design parameters (build-up curves, overall dimensions for full scatter, dose distributions)
- MC calculated correction factors (vacuum gap, inhomogeneity, volume averaging)
- Summary



Current calibration method: air kerma based approach (lonometry)

- Reference air kerma rate (RAKR) of brachytherapy photon source measured with primary standard cavity chamber
- Source strength in terms of Gy/s at 1 m
- Conversion from RAKR to absorbed dose to water using AAPM TG-43 protocol

Calibration set-up



Nucletron micro-Selectron source





Alternative measurement method: absorbed dose based approach (Calorimetry)

- Objective: avoid conversion of RAKR to absorbed dose
- Overall standard uncertainty in conversion using TG-43 is estimated to be 5% (clinically significant)
- Development of a prototype calorimeter for HDR brachytherapy sources
- Direct measurement of absorbed dose

$$D_{\text{point}} = \frac{E_{rad}}{m} = c_p \Delta T$$



EGSnrc Monte Carlo simulations

• Various aspects of calorimeter modelled with DOSRZnrc

AISI 316L

- Default settings used (incl. PRESTA-II)
- ECUT = 10 keV, PCUT = 5 keV
- All calculations to ≤0.1% standard uncertainty
- Source (Nucletron microSelectron Classic):
 - Bare ¹⁹²Ir spectrum used for ¹⁹²Ir cylinder
 - Source encapsulation and steel cable: AISI 316L stainless steel



5.0 mm



MC geometrical inputs DOSRZnrc model for calorimeter

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Nucletron microSelectron Classic Ir-192 source in water and graphite



Water equivalent radial distance R, cm

- $(\mu_{en}/\rho)^w_g = 1.11$ for mean ¹⁹²Ir energy (encapsulated source: 397 keV)
 - Energy dependent \rightarrow calculate fluence spectrum

Scatter build-up along R-axis

20 cm

$ROI = 1 mm \times 1 mm$





0 cm

20 cm

Scatter build-up along Z-axis







0 cm

20 cm

20 cm

Scatter build-up in graphite (1)

- R = 20 cm and $Z = \pm 10$ cm from centre of source
 - → absorbed dose in all 5 ROIs (1...5 cm) >99.5% of D_{full scatter}
- $D_{\text{full scatter}}$ calculated using R = 50 cm and Z = ±50 cm



Scatter build-up in graphite (2)

ROI at R = 1 cm



Radius of graphite cylinder R, cm



Scatter build-up in graphite (3)

ROI at R = 5 cm





Scatter build-up in graphite (4)





Half height of graphite cylinder Z/2, cm



Scatter build-up in graphite (5)

ROI at R = 5 cm, radius of graphite cylinder = 20 cm



Half height of graphite cylinder Z/2, cm



Scatter build-up in graphite (6)

Min. R required at ROI to get 99.9% and 99.5% of D_{full scatter}



Scatter build-up in graphite (7)

Min. Z/2 required at ROI to get 99.9% and 99.5% of D_{full scatter}



Dose distribution parallel to long source axis (1)

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5,000,000,000 histories in less than 1.5 hours

Variance reduction techniques used

- Electron range rejection Here: ESAVE = 0.871 MeV
- Photon cross section enhancement Increase photon cross section of selected region in geometry by factor C_e → this will increase the interaction density by that factor



Dose distribution parallel to long source axis





Variation of D_{average} with core height

Daverage (core height) / D_{full scatter} at ROI





Core height required to measure $D_{total} = 99.5\%$ of $D_{full scatter}$

ROI (cm)	Max. core height, cm
2	0.5
3	0.75
4	1.05



Radial dose gradient in graphite

Dose vs distance (ROI = 2 cm)



NPL

Summary of MC simulations

Source to core, cm	Build- up	Min. R, cm	Min. Z/2, cm	Max. core height, cm	Dose gradient over 2 mm, %	Dose rate from 370 GBq source, Gy/s	∆T in 120 s, K	
1	X	√	√	X	X	9.99E-02	1.68E-02	
2	(✓)	8.1 5.4		0.5	23	2.52E-02	4.24E-03	
2.5	 Image: A second s	10.1	6.8	0.6	18.5	1.60E-02	2.69E-03	
3	✓	12.1	8.1	0.75	15	1.12E-02	1.88E-03	
4	4 🗸		10.9	1.05	11	6.21E-03	1.04E-03	
5	5 🖌		X	\checkmark	\checkmark	X	X	



Volume averaging factor

- Centre of ROI: 25 mm from source
- Dose at a 'point', *D_{point}* size: 0.1 mm × 0.1 mm
- Dose averaged over core, *D_{core}* size: 2 mm × 5 mm







point $k_{\rm av}$ =1.0033core

Inhomogeneity correction factor

- Centre of ROI: 25 mm from source
- Dose averaged over core, *D_{core}* size: 2 mm × 5 mm
 - = graphite
 = air
 = aluminium or steel





$$k_{\rm inh} = \frac{D_{\rm core, graphite}}{D_{\rm core, graphite+air+metal}}$$



Inhomogeneity correction due to aluminium tube

Percentage change of dose to core due to absorption and scatter in aluminium tube



Inhomogeneity correction due to stainless steel tube

Percentage change of dose to core due to absorption and scatter in stainless steel tube





Gap correction factor



Displacement correction, Z-axis

	an ann an											-	and the second
EGS file name:	TS0034	see also TS0032				Source centr	red.						
						z = 7 cm							
Core height Z: 0.5 cm, o	ore thickness: I	0.2 cm											
Centre-to-centre source	+to-core: 2.5 cm												
Geometrical inputs													
	R												
radii (cm)													
10	11	102	103	104	105	106	107	108	109	110	111		
2.96	10		93	94	95	96	97		99	100	101		
2.7	9	82	83	84	85	86	87	88	89	90	91		
2.6	8	72	73	74	///////////////////////////////////////	///////////////////////////////////////	//////	///////////////////////////////////////	79	80	81		
2.4	7	62	63	64	65	66	67	68	69	70	71		
2.3	6	52	53	54	55	56	57	58	59	60	61		
2.04	5	42	43	44	45	46	47	48	49	50	51		
0.165	4	32	33	34	35	36	37	38	39	40	41	0.1cm	aluminium
0.065	3	27	23	24	25	26	27	28	29	30	31		
0.055	2	12	13	14	15	16	17	18	19	20	21		
0.03	1	2	3	4	5	6	7	8	9	10			
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=	aluminium												
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=	photon cro	ss section enhancement in th	is region; mini	mum dis	tance from blue lir	ne to ROI = CS	5DA ran	ge of 0.9	HeV ele	ctrons in graph	ite = 0.26 cm (ICRU report 37)		







Displacement correction factor, R-axis





Summary: Design criteria for prototype calorimeter

- Graphite cylinder (R = 10 cm, Z = 14 cm)
- Centre-to-centre source-to-core distance: 2.5 cm
- Thickness of core: 0.2 cm
- Height: 0.5 cm
- Mass: 2.67 g
- Aluminium tubing with max. 1 mm radial thickness,
 0.2 mm radial clearance
- 1 mm vacuum gap around core to deal with measurement problems due to self-heating of source

