



Underwater noise due to marine machinery

Alistair Mackinnon





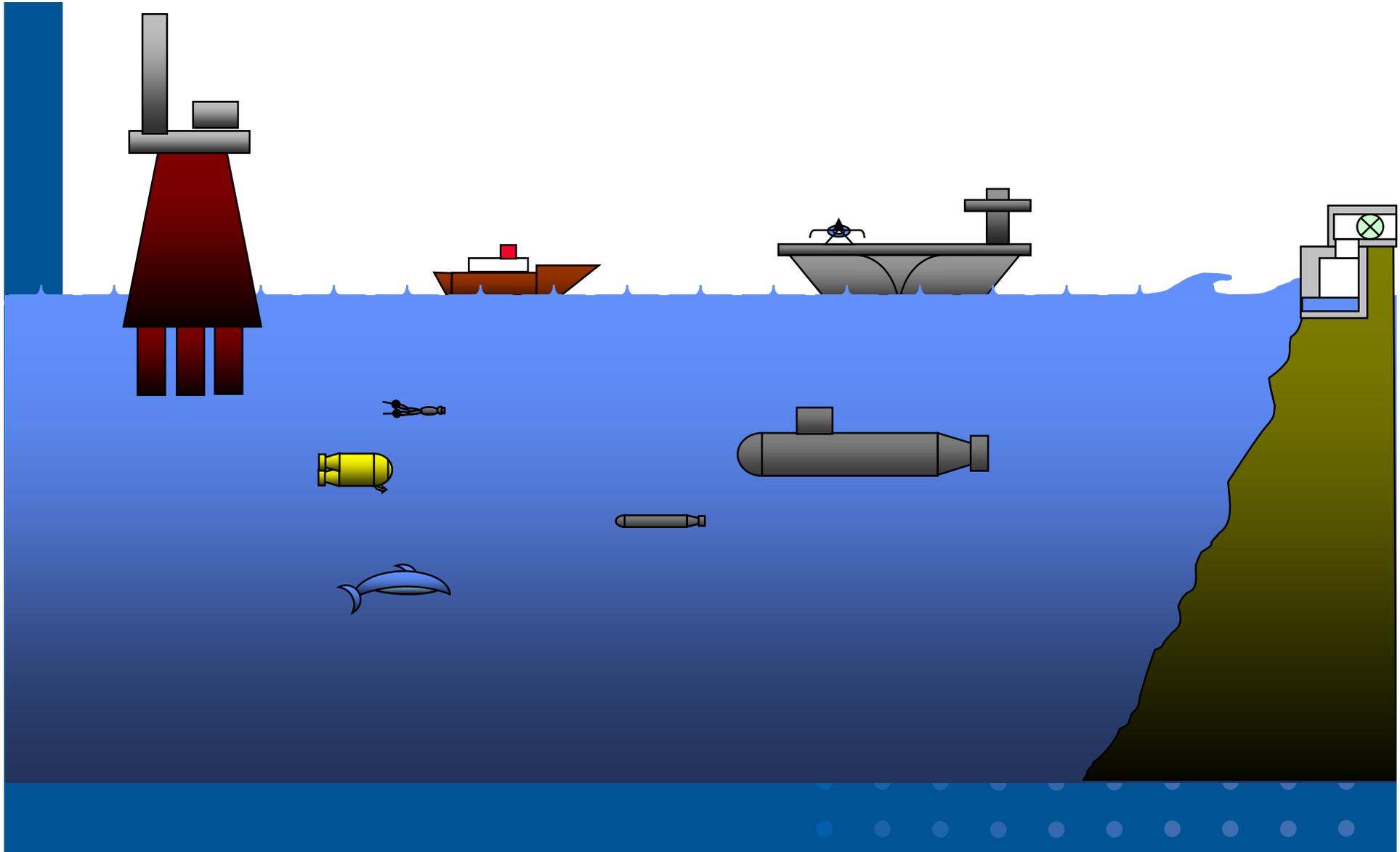
Acknowledgements

Richard (Dick) Whitson – NEL

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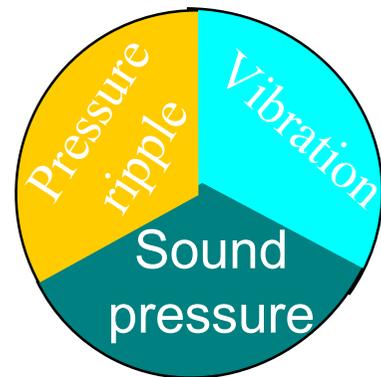
Overview



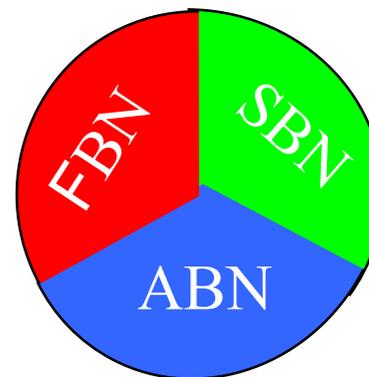
Three types of problem



- Habitation issues (people)
- Self-noise issues (equipment)
- Environment or stealth issues



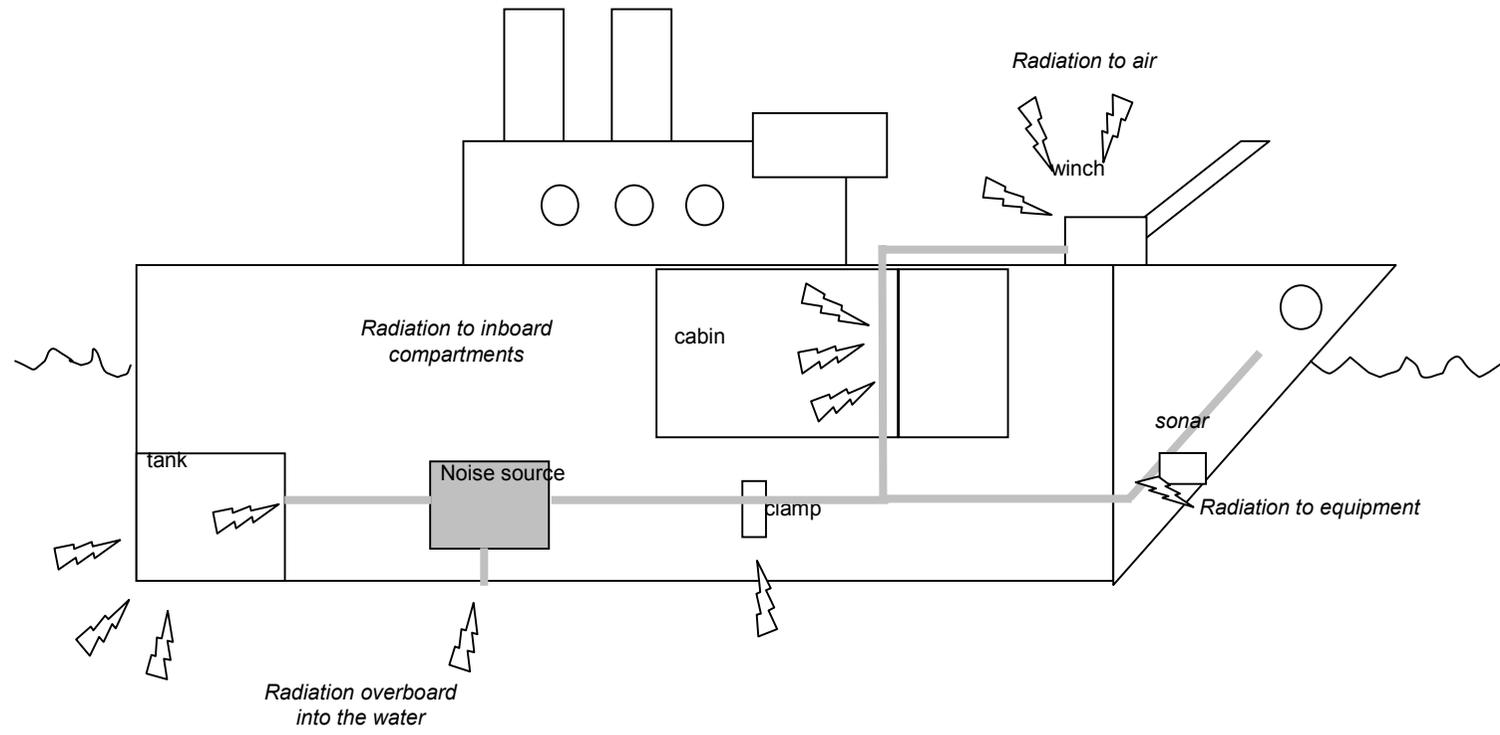
measurement



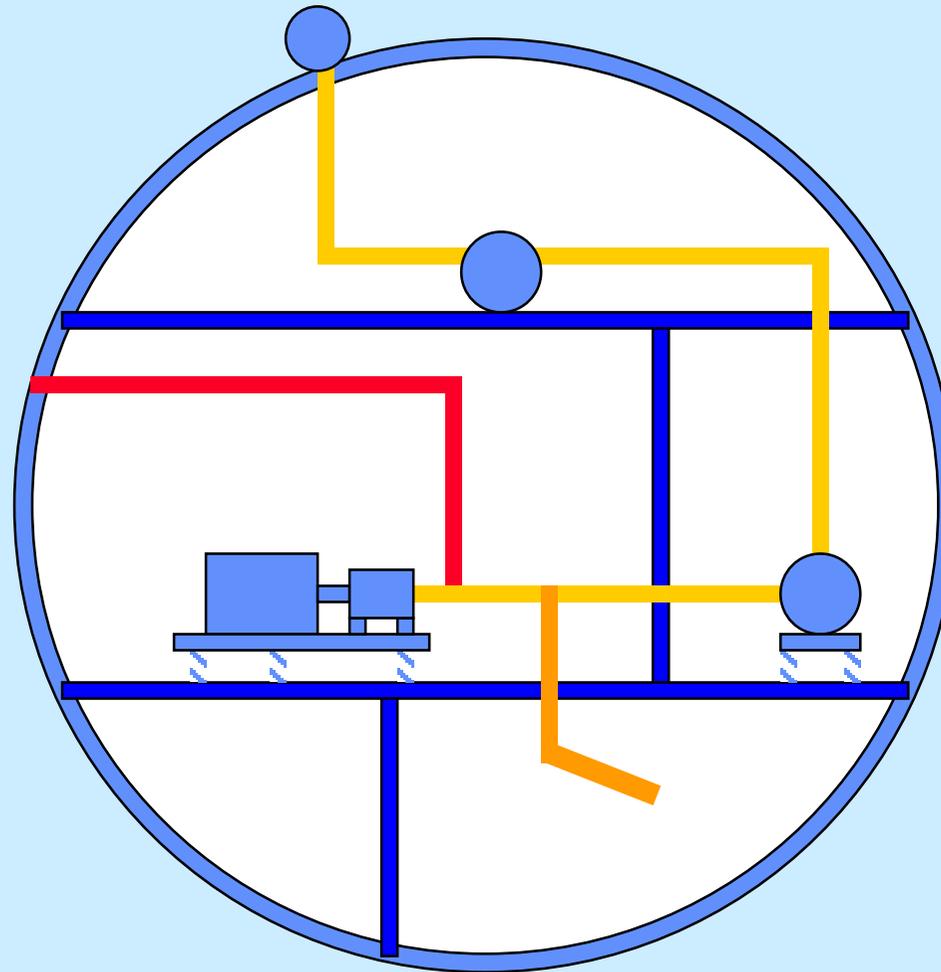
path



What is FBN



Machinery noise

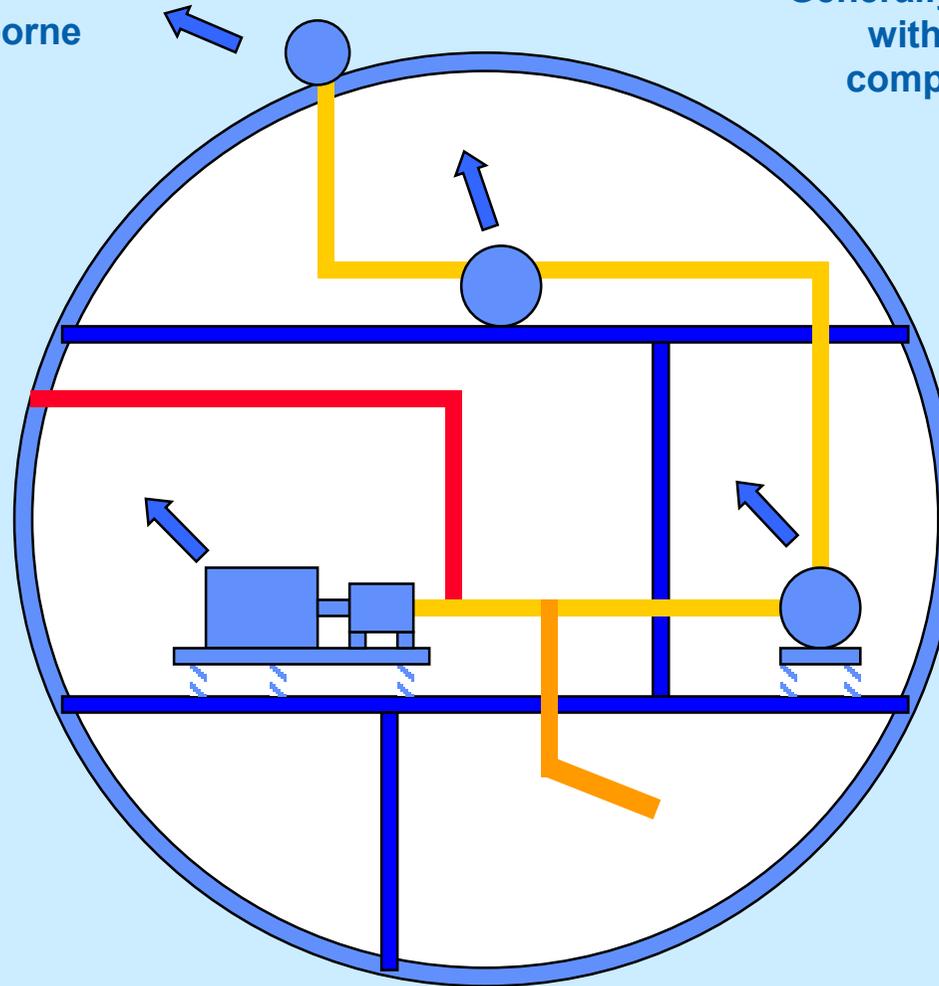


Airborne noise (ABN)

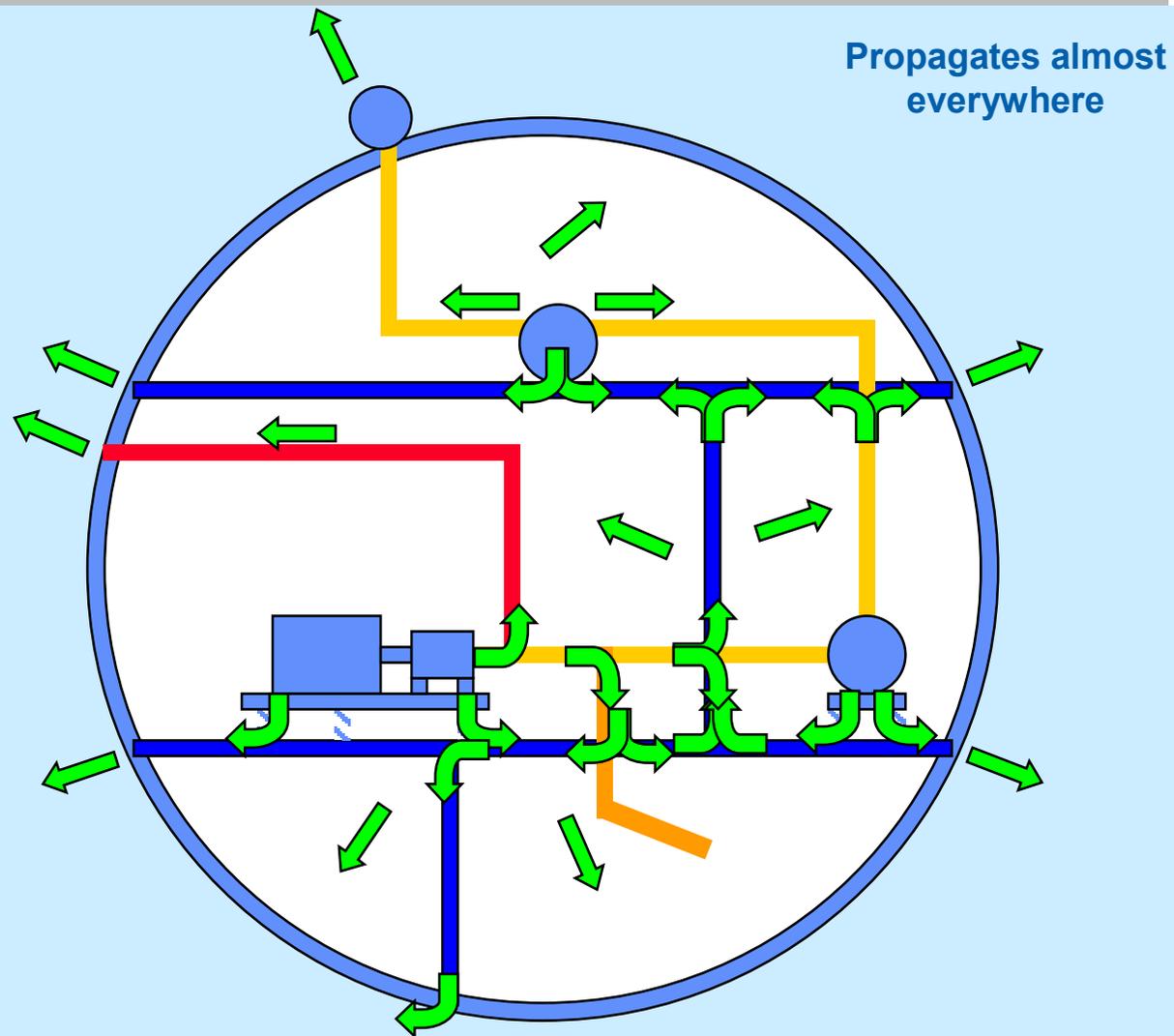


Water borne
Noise

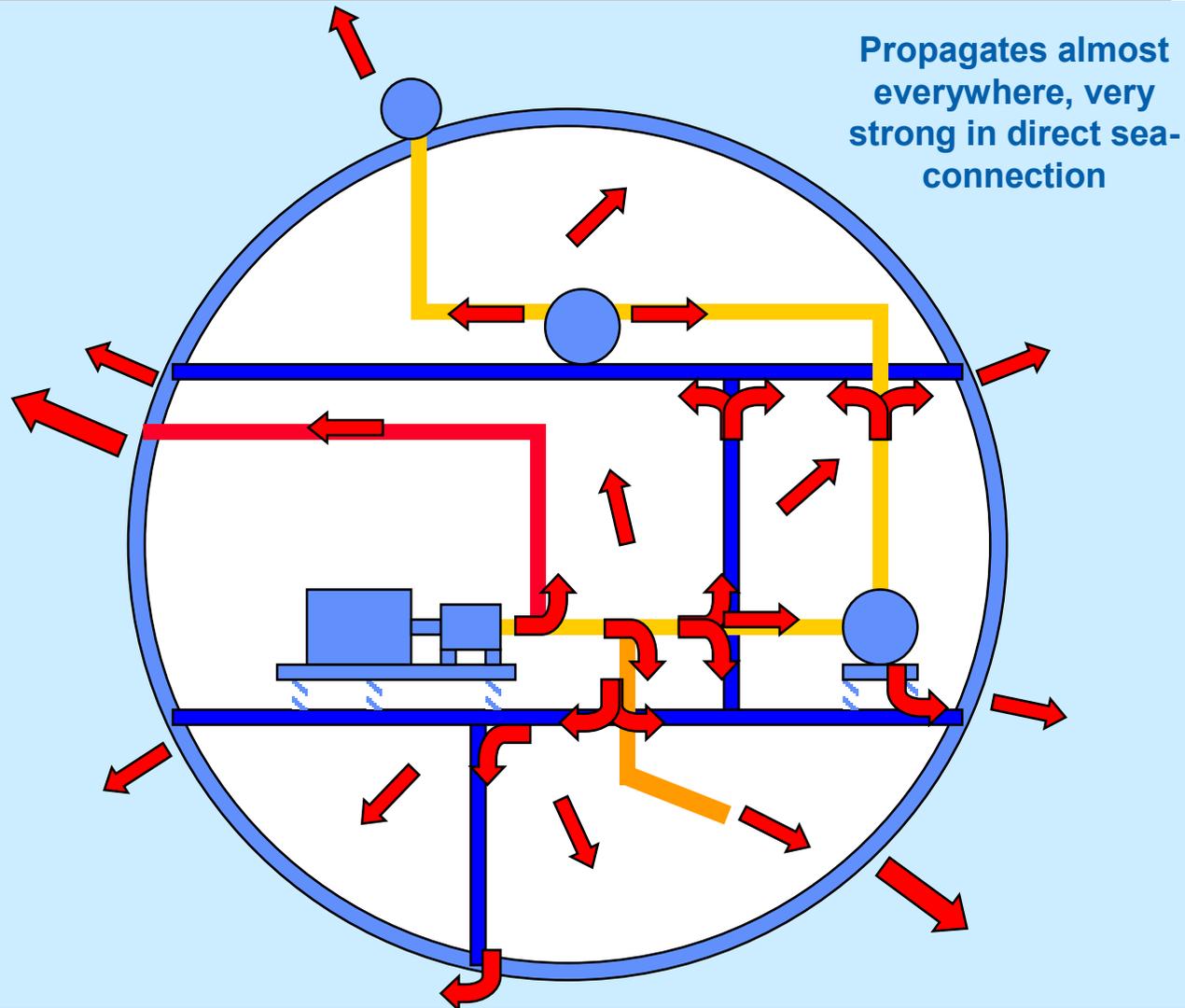
Generally contained
within own
compartment



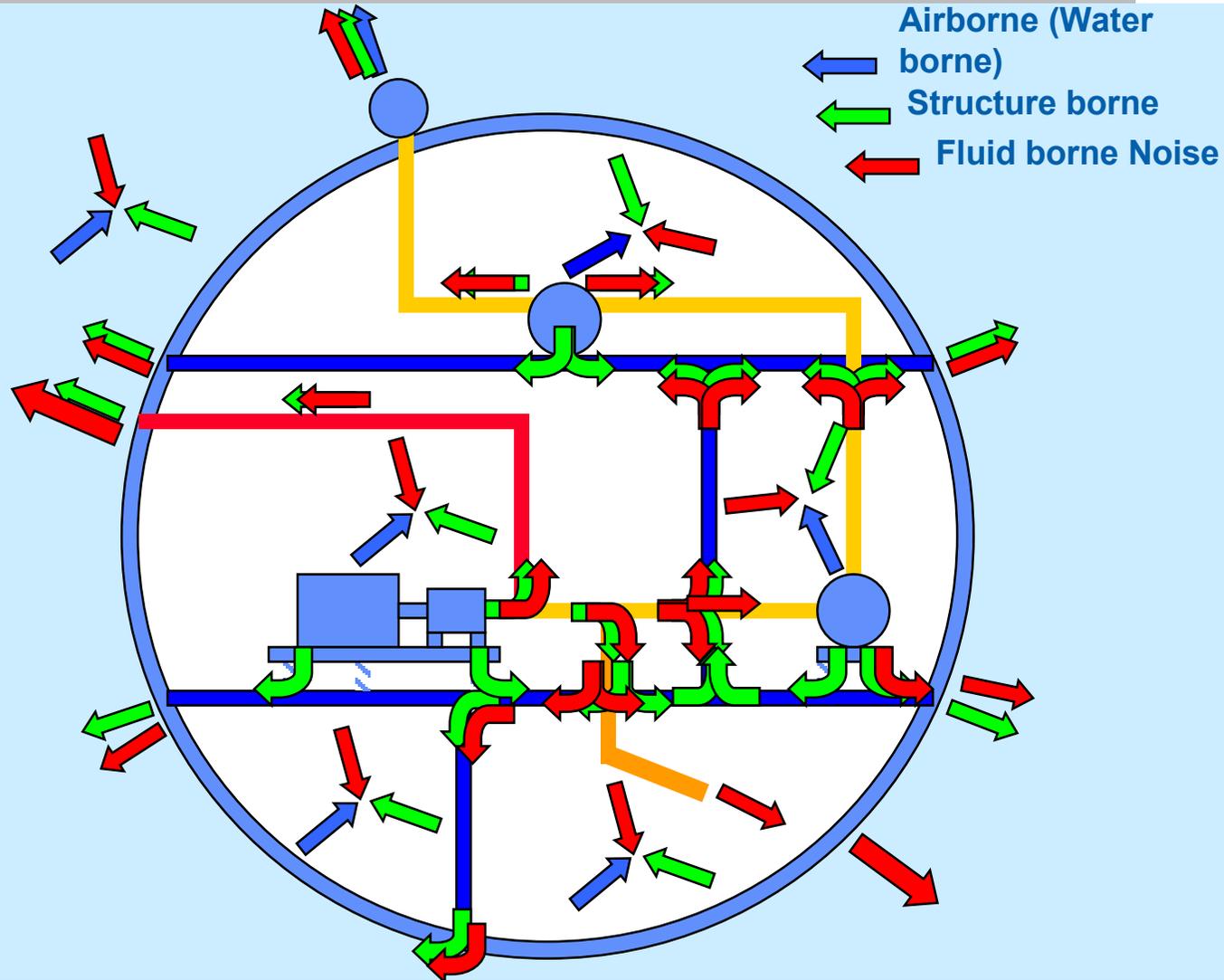
Structure borne noise (SBN)



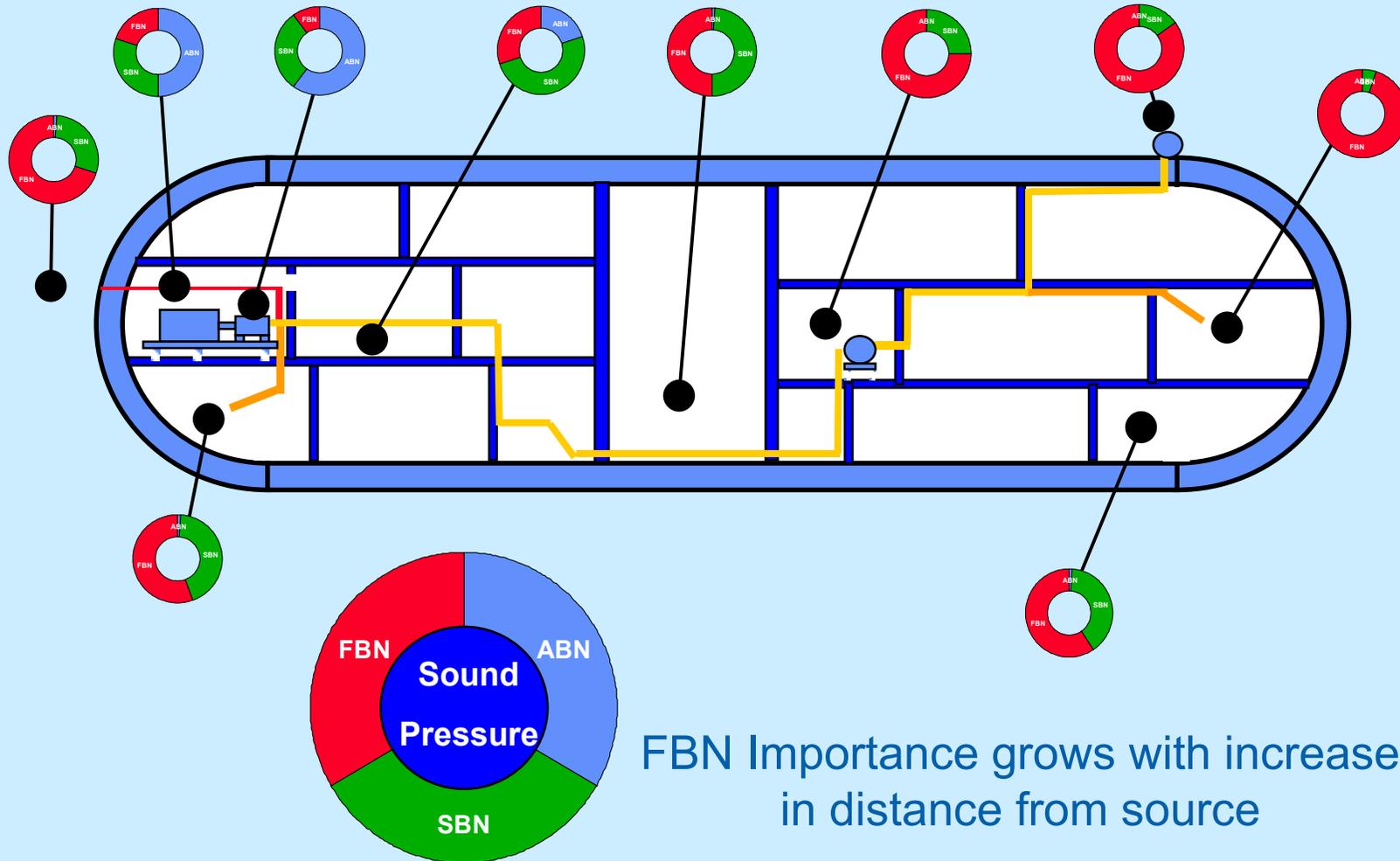
Fluid borne noise (FBN)



Multiple paths

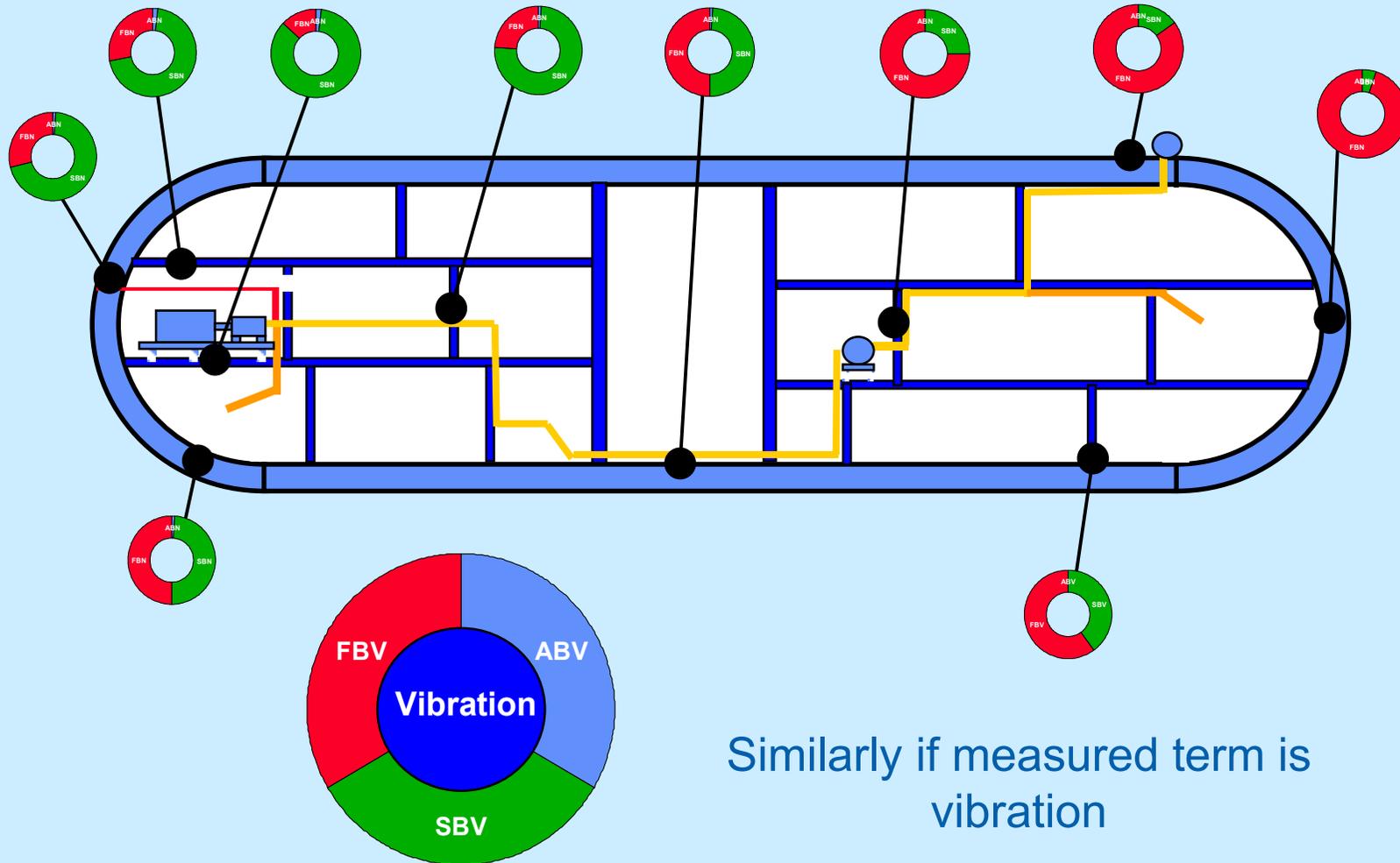


Sound pressure

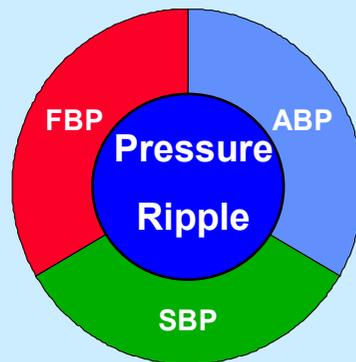
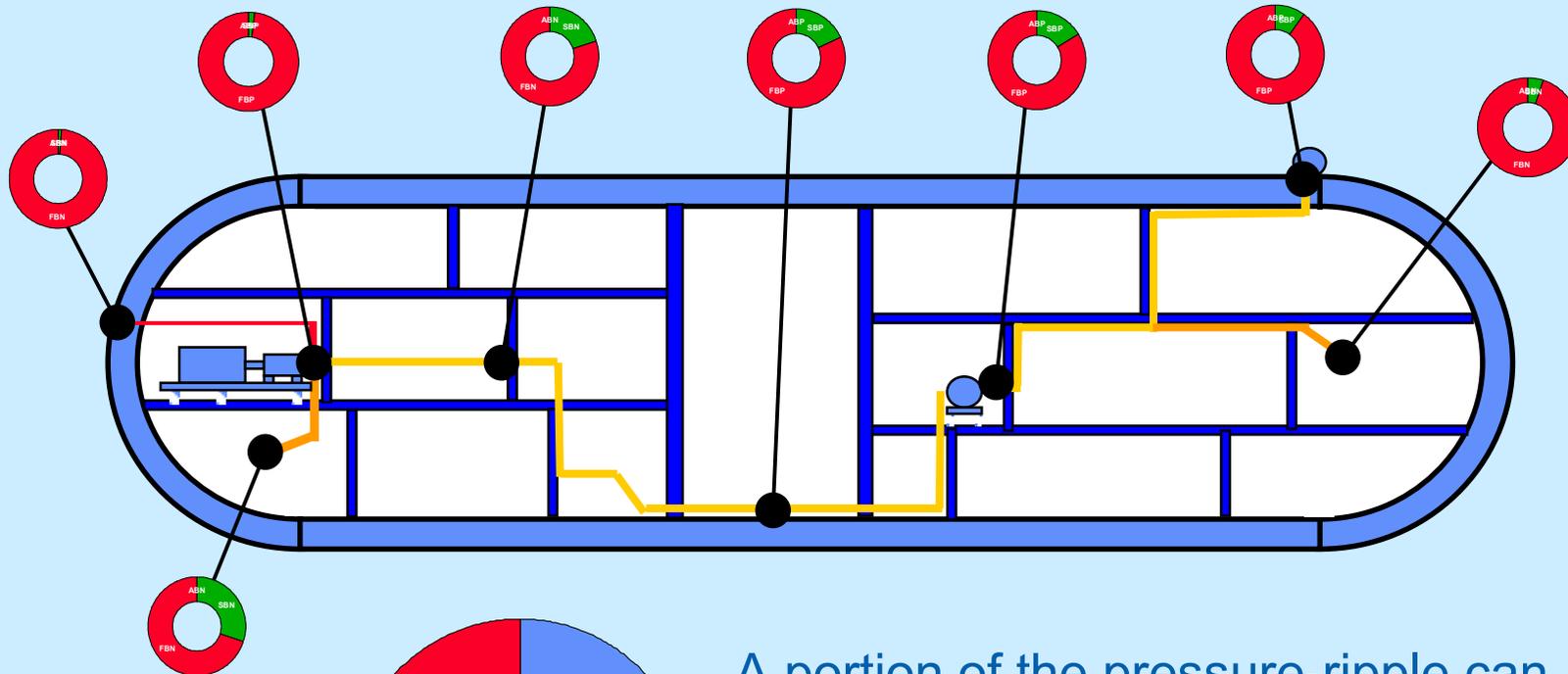


FBN Importance grows with increase in distance from source

Vibration



Pressure ripple



A portion of the pressure-ripple can be due to fluid-structure-fluid energy exchange. This can be important downstream of attenuators and valves



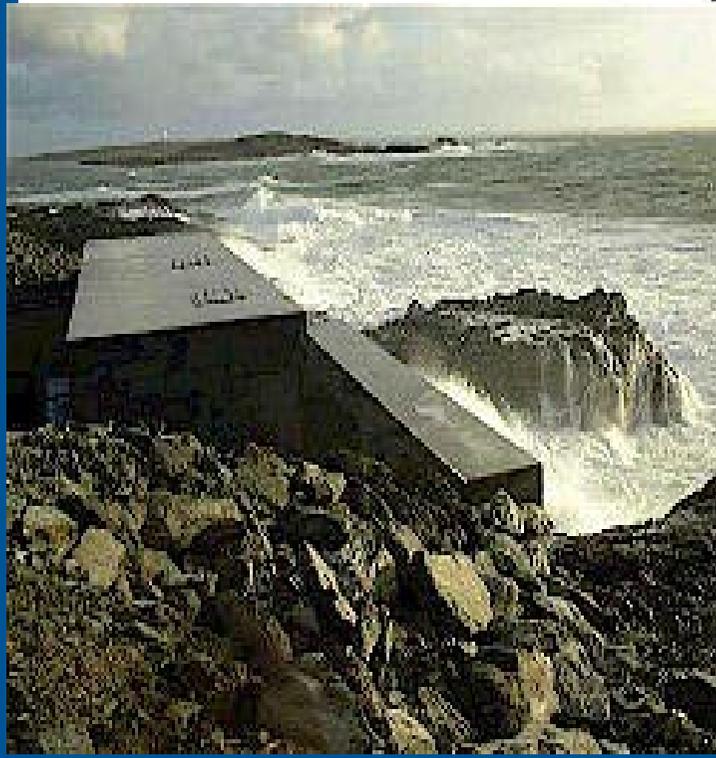
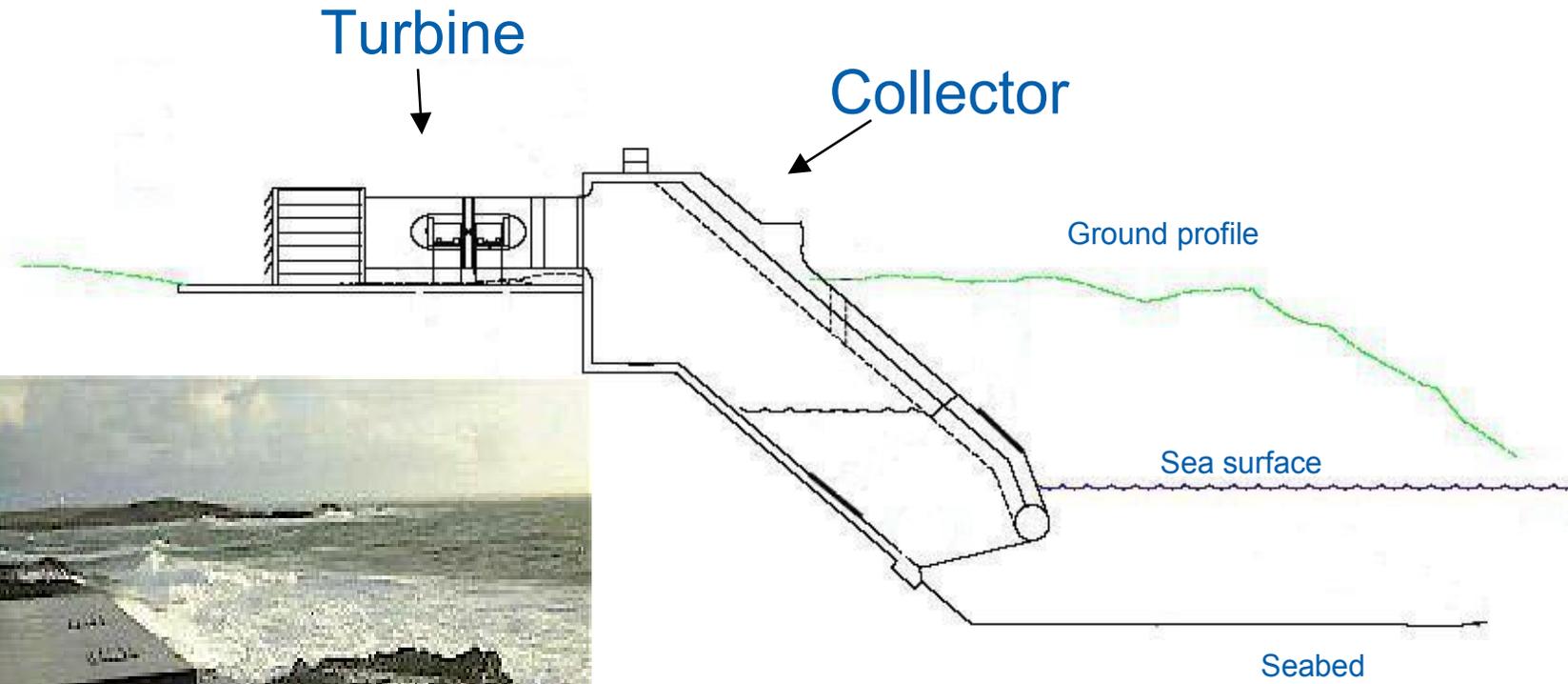
Machinery noise



- In-pipe pressure-ripple measurement and measurement of FBN
- Fluidborne noise attenuators
- Non-invasive measurement using PVDF
- Pump Noise
- Valve Noise



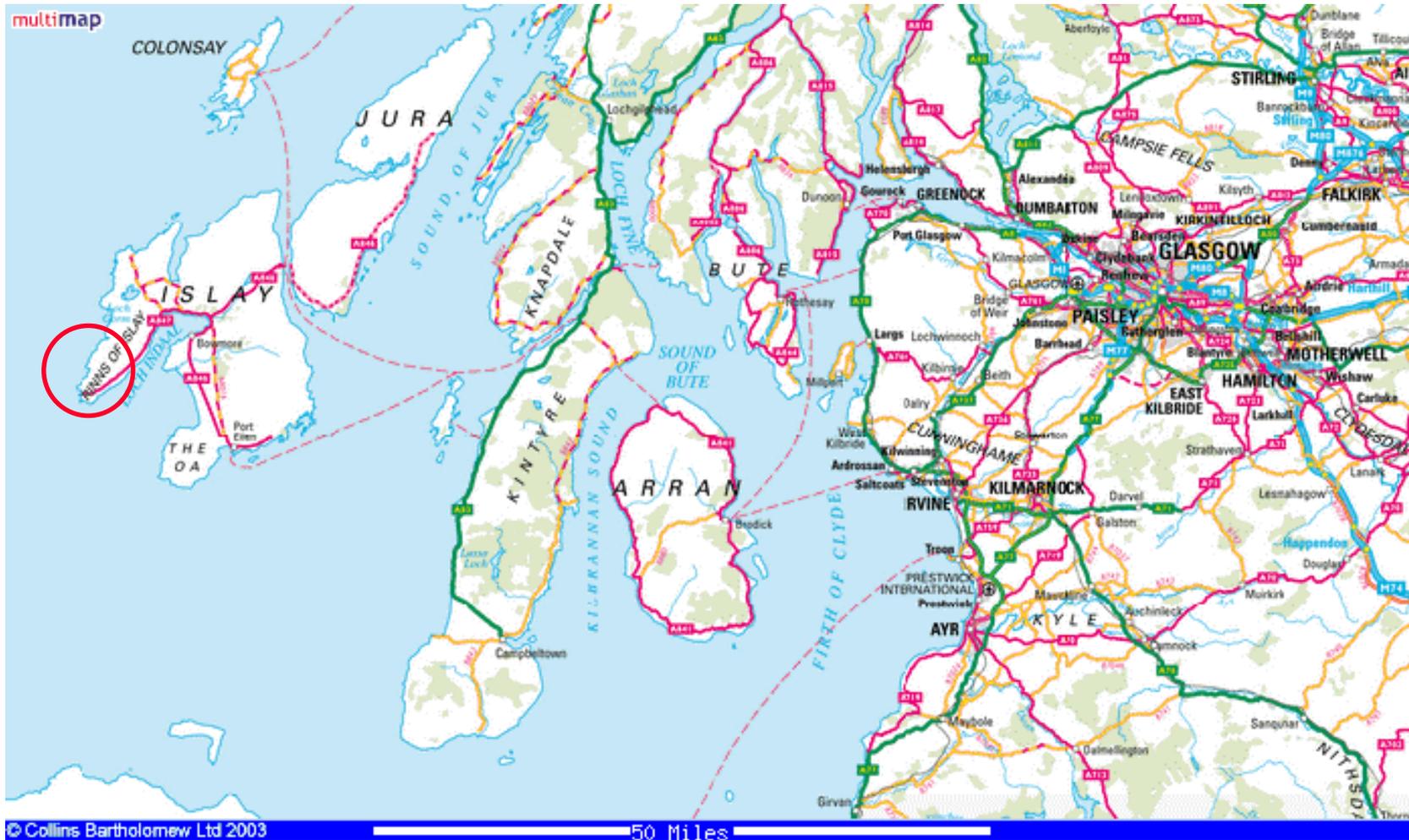
WAVEGEN 'LIMPET'



- Land Integrated Marine Power Extraction Turbine



Location



Objectives



Assess challenges in measurement of:

- Audible noise
- Ground borne vibration
- Underwater noise

Working towards a simple means of quantifying Emission and Immission levels from shore based wave power plant



Measurement approach



Measure source strength (Emission)

- Variation with available power (sea-state) & generated power

Measure background (ambient) noise at source & receiver

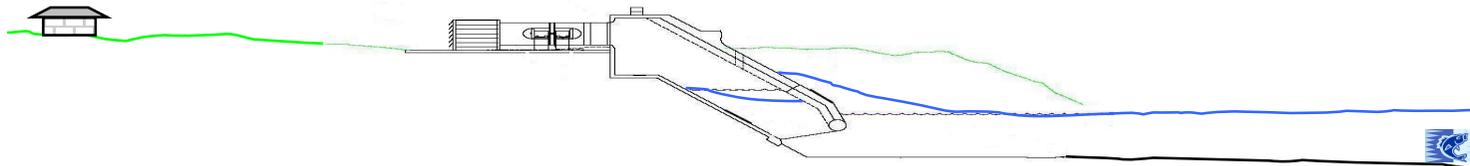
- Variation with available power (sea-state)

Predict levels at a distance (Immission)

- Hemispherical propagation for audible noise (ü) and vibration (?)
- Hemicylindrical propagation from inlet mouth for underwater noise

Compare against local background (ambient) noise & targets (?)

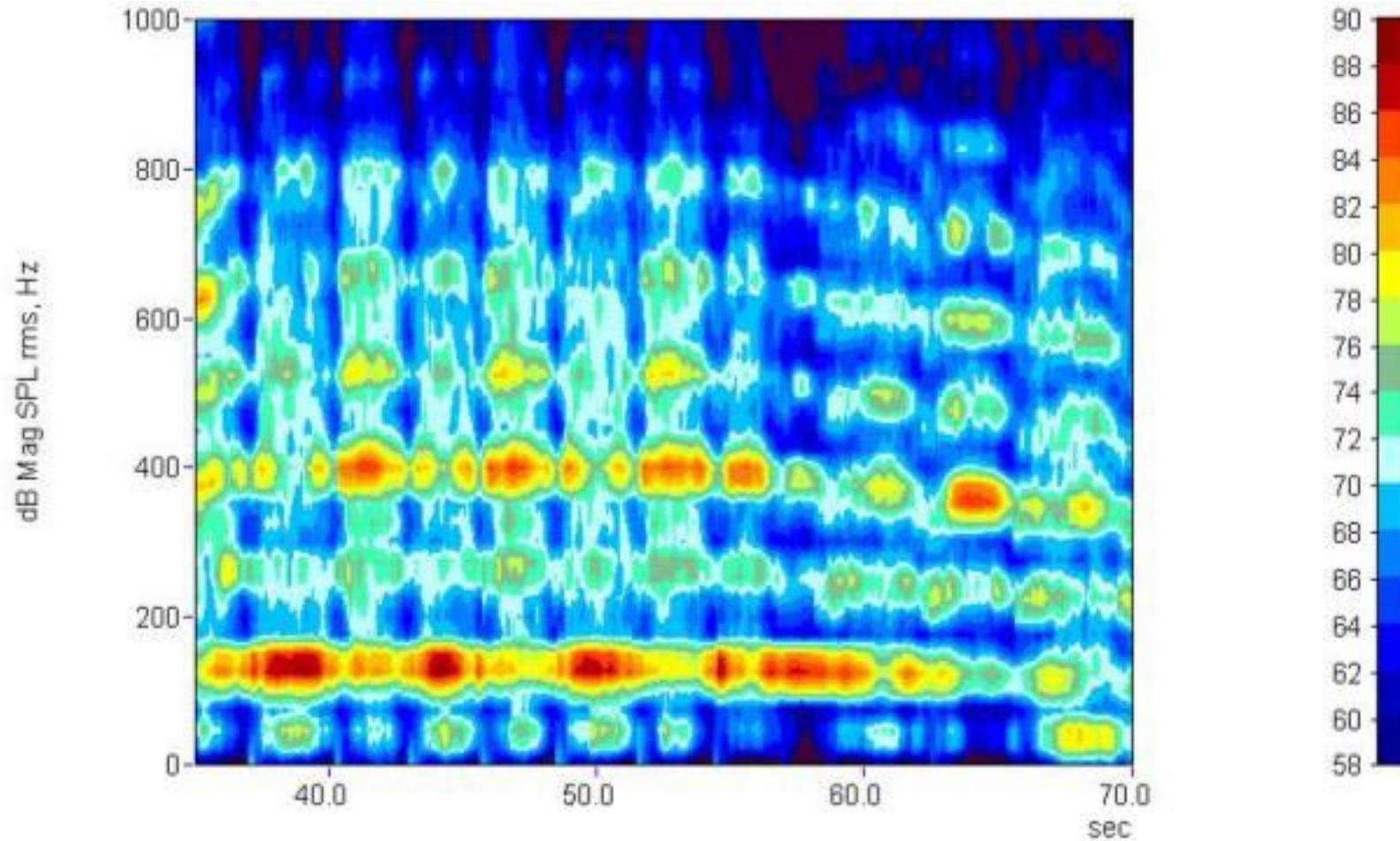
Quote at reference positions (e.g. plant boundary, shore edge, gulley mouth)



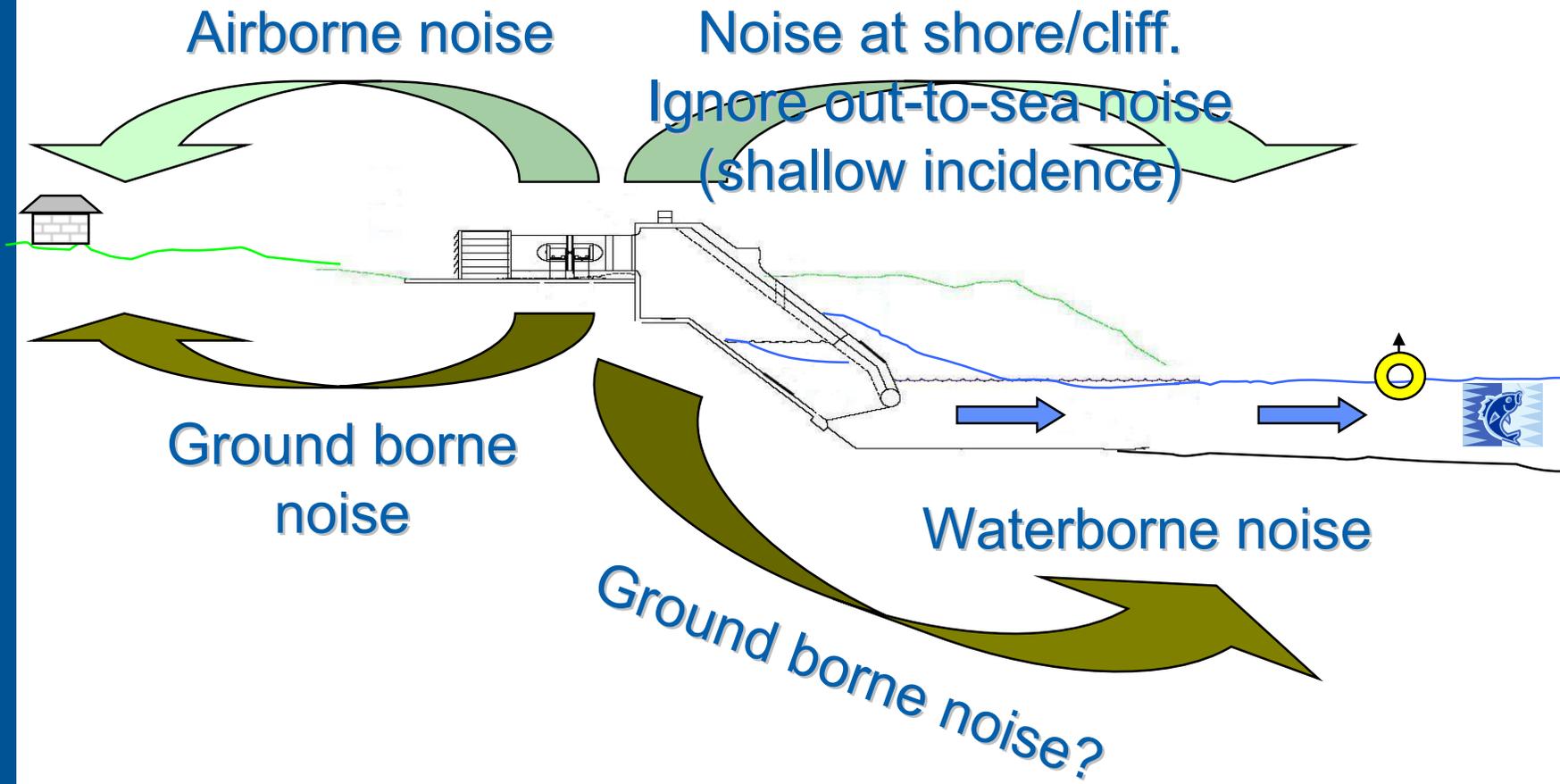
Random cyclic variation



Audible noise variation with time 3 m from bell-mouth



LIMPET Device

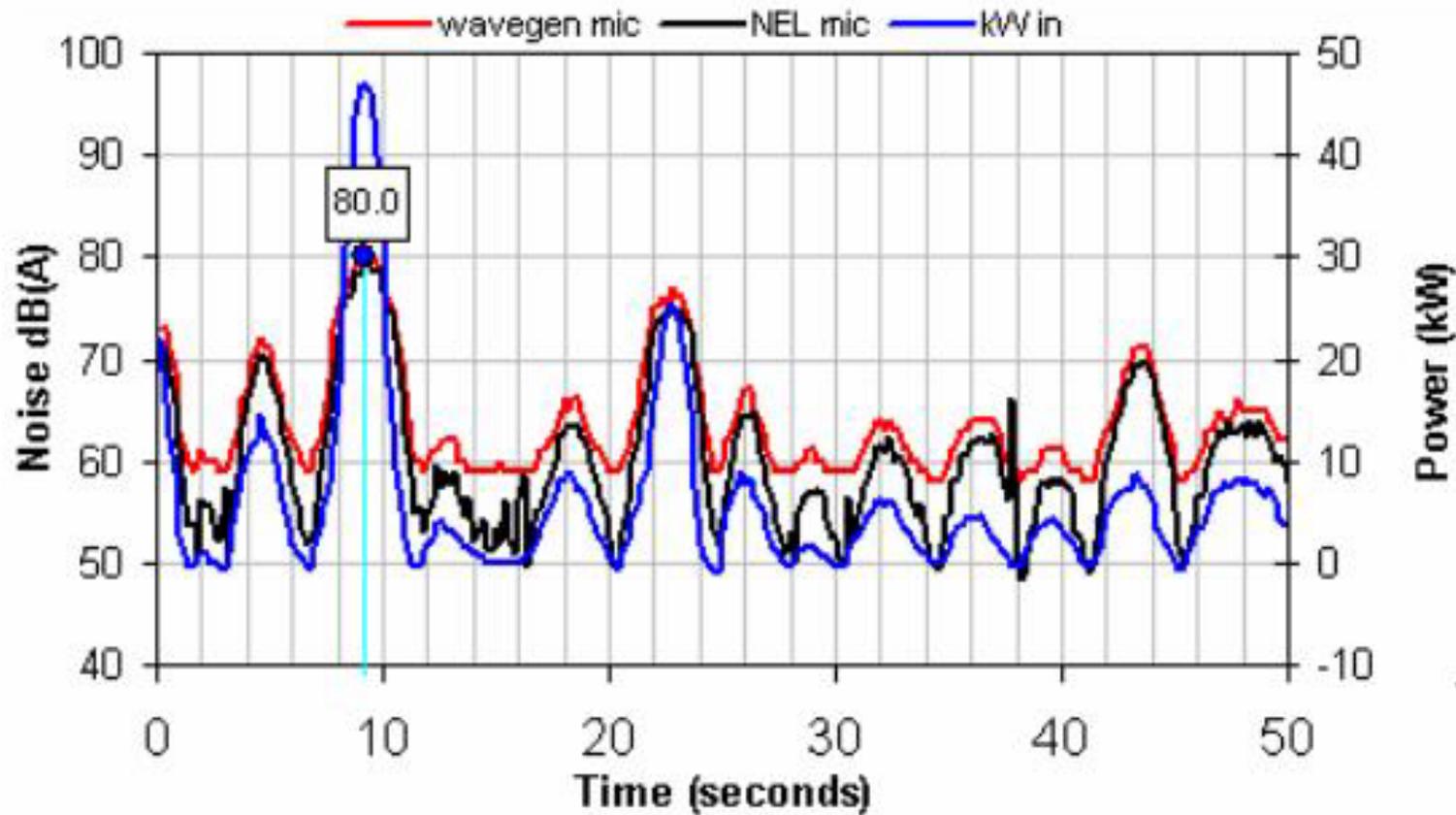


Audible noise & wave power



Use audible noise at a fixed position as a 'reference' position

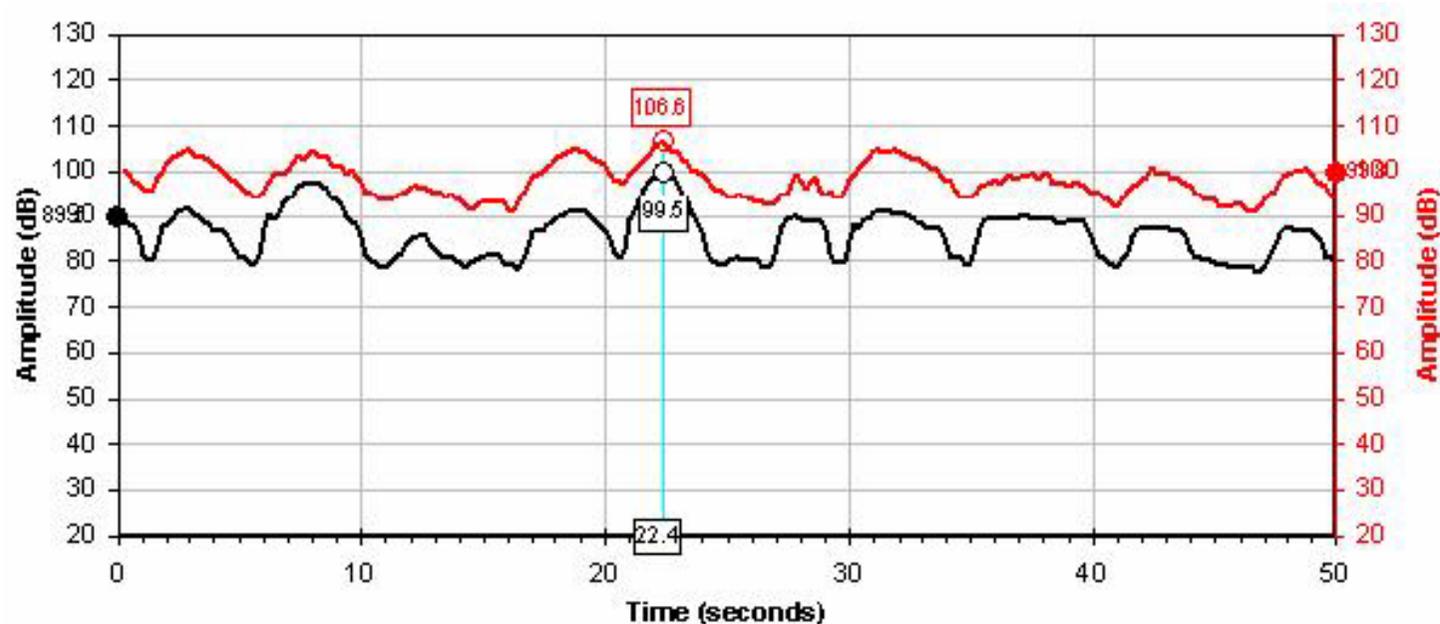
Plot variation against a 'roving' measurement position



Audible noise inside & out

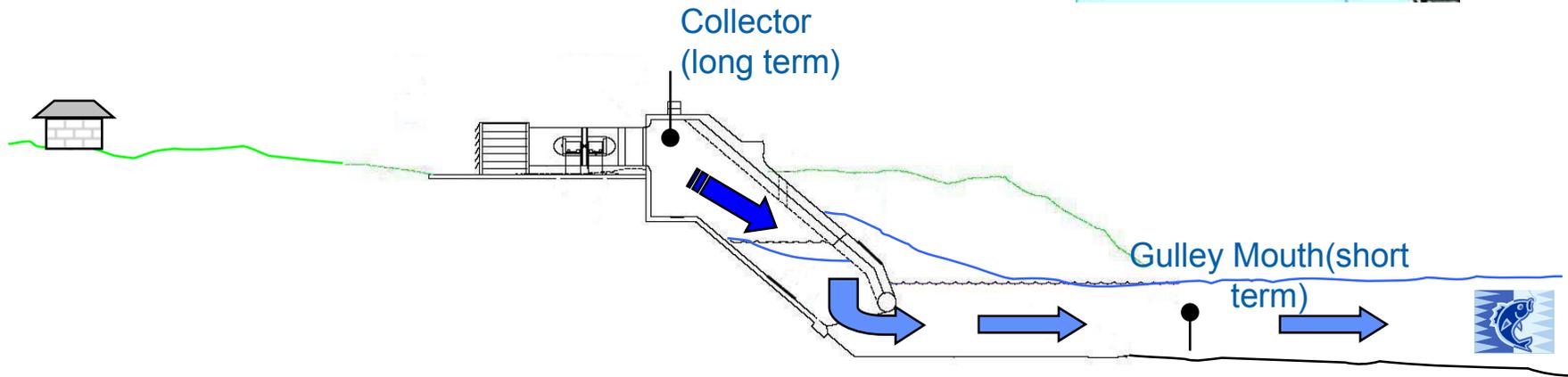


- Plan to use a hydrophone inside the collector air space for long-term monitoring due to deployment and reliability issues
- Good agreement between Audible noise at reference position and hydrophone inside collector



- Agreement between hydrophone at gulley mouth and inside collector still to be shown

Measurement underwater



Waterborne noise



Measurement – underwater



Emission (generated noise)

Machinery Noise

- Lp in collector (Hydrophone)
- Lp at gulley mouth (Hydrophone)
- Show relationship between two (possibly $L_{p,m} = L_{p,c} + 6\text{dB}$)
- Derive Ls, Source Level dB(/Hz?) re 1 μ Pa at 1m

Sea-slap/wave

- Different from background ?
Assume it is not ?

Immission (received noise)

Based on simple hemi-cylinder propagation calculation to 100m from gulley mouth:

$$L_{p,100m} = L_{p,m} - 13.5 \text{ dB}$$

(based on an average depth of say 15m)

Or, simply based on Lp,m at gulley mouth



Thresholds underwater



Health of Fauna Nuisance to Fauna Significant Biological Impact

- Actual discomfort, damage or death
- Interference with the use of hearing for feeding or communication reducing viability
- Disturbance of breeding behaviours reducing viability

Emission & Immission concepts are still relevant:

- Emission is given by Source Level, L_s , in dB(/Hz?) re $1\mu\text{Pa}$ at 1m
- Immission is received Sound Level in dB(/Hz?) re $1\mu\text{Pa}$
- **SPECTRAL DENSITY ? Not 1/3rd OCTAVE: Big difference at high f. Need to take care when source consists of tones.**

MarLIN Benchmark (for “received” pressure level i.e. Immission):

- 130 dB(/Hz?) re $1\mu\text{Pa}$ at 100m, 45-7100 Hz

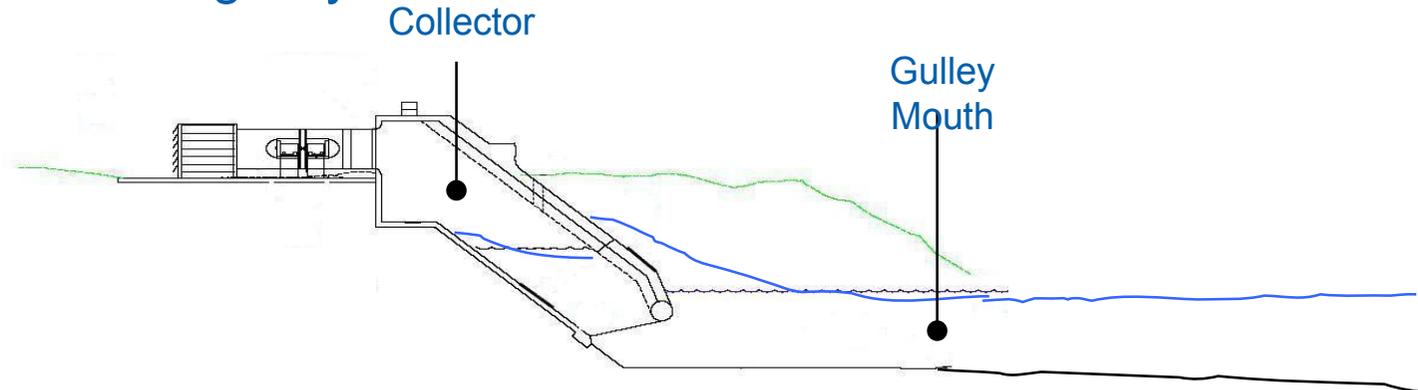
ICES levels (for radiated noise of fisheries research vessels) 1Hz-100kHz, 11 knots

- 135 dB/Hz re $1\mu\text{Pa}$ at 1m at 10Hz, 130 dB/Hz at 1kHz, 93dB/Hz at 50 kHz

Simplified target?



- Take 130 dB re $1\mu\text{Pa}$ as the underwater target at the mouth
- This equates to $130 - 32 = 98$ dB re $20\mu\text{Pa}$ as the target for the sound pressure level in the Collector. This assumes the collector area = the gulley mouth inlet area

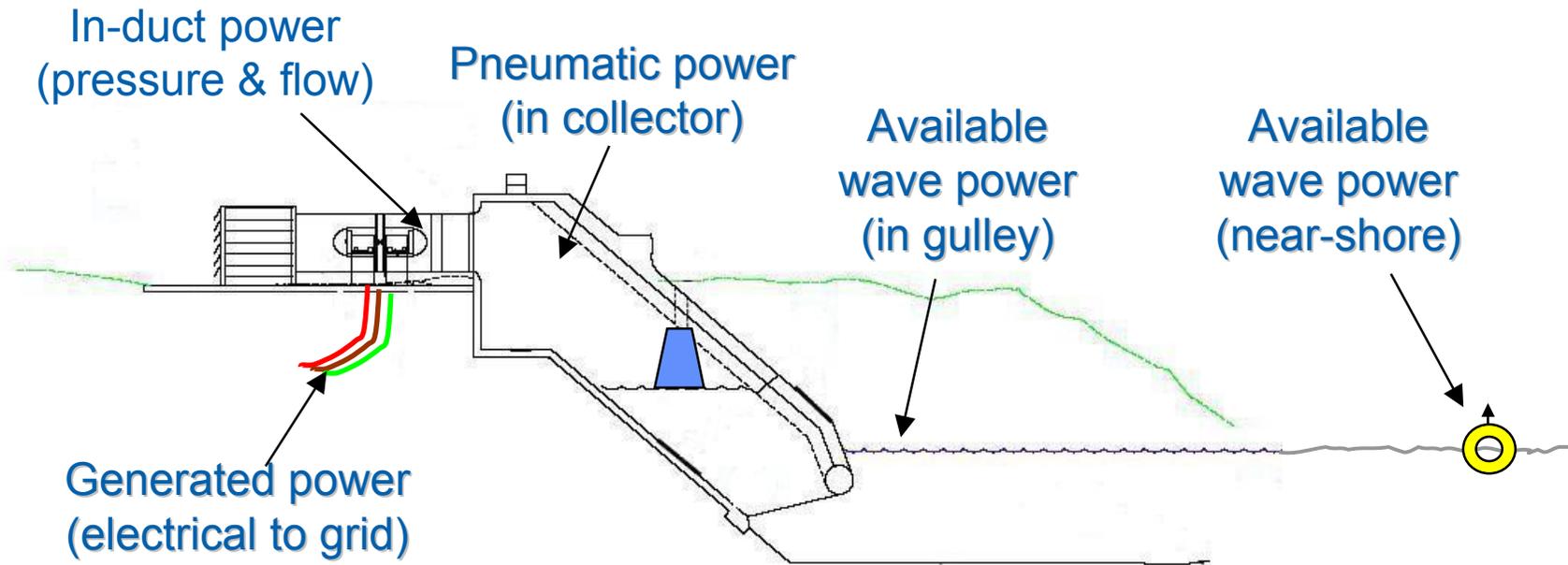


- 32 dB correction calculated from simple acoustic theory for an air-water interface (6dB) plus change to dB re $20\mu\text{Pa}$
- Note: These are band levels; if these are in dB/Hz then a significant increase in level will be allowed if 1/3rd Octaves are used. Safest route is to use 98 dB re $20\mu\text{Pa}$ as the band total

Measurement - Power

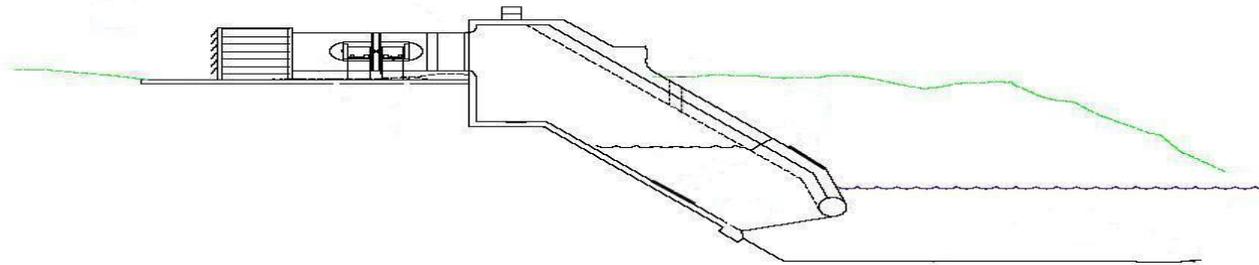


Four (or 5?) forms of power



- Audible noise, vibration and underwater noise all need to be compared against some form of background versus an independent parameter
- Available wave power (near-shore or gully?) is obvious choice since background noise and vibration will be most closely related to this

Overview – Long Term



- Standardise on 10 minute (?) averages of:
 - Audible noise, underwater noise and vibration at reference positions
 - Generated power and turbine speed
 - Sea-state, available wave power, wind speed & direction
 - Background noise (audible, vibration and underwater) with turbine stopped
- 10 min averages can be made up from numbers of shorter averages
- L_{eq} , L_{10} and L_{90} with occasional 1/3rd Octave spectra may be of benefit
- This will allow plotting of parameter against available power

