

Towards Miniaturisation of UWB Antennas

X. Chen, L. Guo, S. Wang, C. G. Parini

Department of Electronic Engineering
Queen Mary, University of London, U.K.

Overview

- Introduction
- Antenna Size and Bandwidth
- Miniaturised Planar UWB antennas
 - Monopoles
 - Half Disc Monopole Antennas
 - Tapered Slot Antennas
- Discussion

Introduction – QMUL Antenna & EM Group

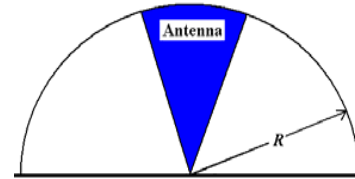
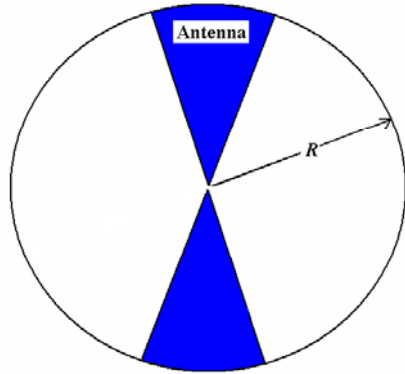
- **The group was found in 1968**
 - Currently: 5 Academic Staff, 8 RAs and 18 PhD students;
 - Funding over this RAE period: > 4M; Current EPSRC funding: >1.39M;
 - Wide links with industry and institutions
- **Research topics**
 - Covering wide areas in antenna engineering and EM applications
- **Facilities:**
 - 3 Anechoic Chambers (500 MHz – 350 GHz),
 - 2 CATRs (5GHz – 350GHz),
 - NSI 0.9m x 0.9m NF scanner.

Introduction – UWB Antennas

- **The quest for small UWB planar antennas**
 - Rapid development of UWB wireless communication systems has led to the increasing demand for miniature UWB antennas.
 - Provide flexibility to device designers and easily integrates into space-limited systems such as home-cinema equipment, Portable computers, PC peripherals, PDAs, mobile phones and UWB USB.

- **Main Effects of Size reduction on Antenna Performance:**
 - Gain, bandwidth and efficiency

Antenna Size and Bandwidth



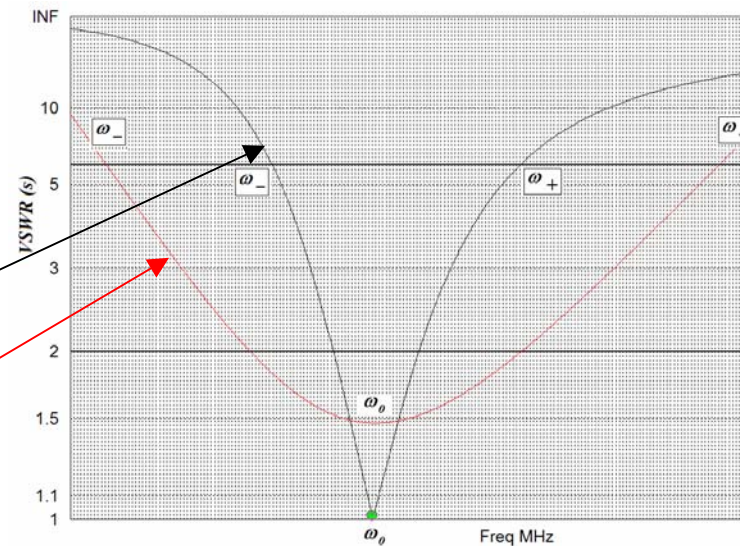
Ground Plane

R is the radius of the boundary sphere around an antenna

$$FBW = \frac{\Delta f_{3dB}}{f_{0dB}} = \frac{1}{Q}$$

Higher Q ,
narrower FBW

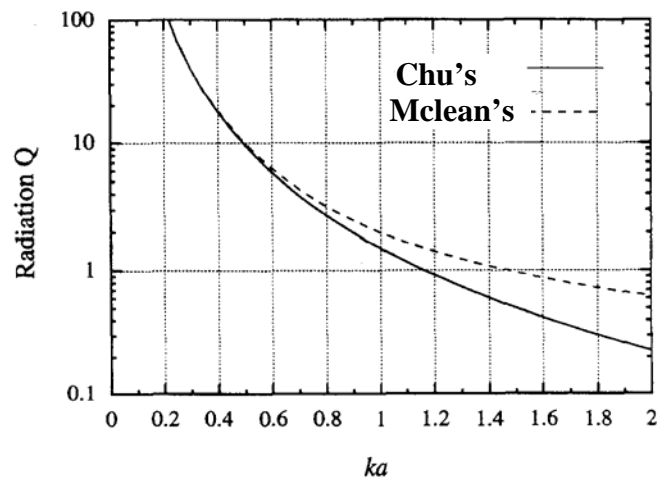
Lower Q , wider
FBW



Antenna Size and Bandwidth

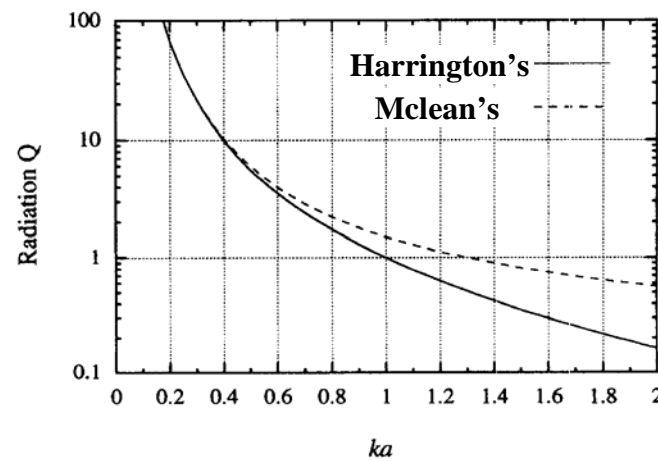
Minimum attainable radiation Q of a **linearly polarized** antenna

$$Q = \frac{1}{(kR)^3} + \frac{1}{kR}$$



Minimum attainable radiation Q of a **circularly polarized** antenna

$$Q = \frac{1}{2} \left(\frac{1}{(kR)^3} + \frac{2}{kR} \right)$$



The lowest values of Q is limited by the size of an antenna!

- [1] L. J. Chu, "Physical Limitations of Omni-directional Antennas," *J. Appl. Phys.*, Vol. 19, pp. 1163-1175, Dec. 1948
- [2] R. F. Harrington, "Effect of antenna size on gain, bandwidth and efficiency," *J. Res. Nat. Bur. Stund.*, vol. 64-D, pp. 1-12, Jan./Feb. 1960.
- [3] J. S. McLean, "A Re-Examination of the Fundamental Limits on the Radiation Q of Electrically Small Antennas," *IEEE Trans. Antennas Propagat.*, Vol. 44, pp. 672-676, May 1996

Antenna Size and Bandwidth

- Both Chu-Harrington and McLean limits indicate that reducing the size of the antenna leads to the decrease of the bandwidth of the antenna.

Challenge: Reducing antenna size while retaining UWB property!

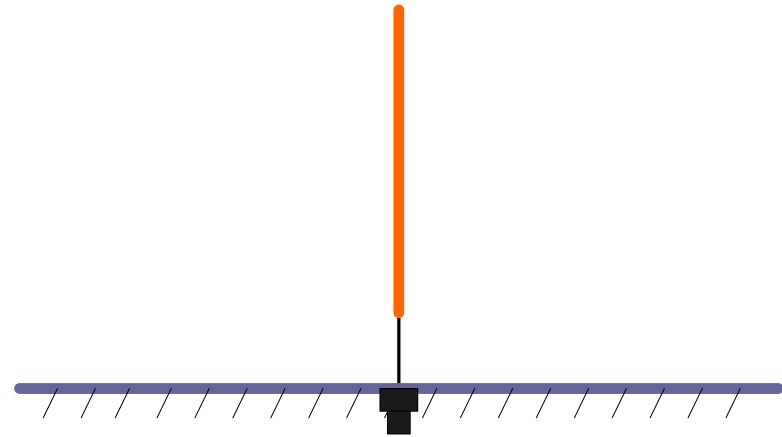
- In practice, a variety of fat element monopoles were found to provide broad impedance bandwidth!

Monopoles

Classical Broadband Antennas

Straight wire monopole

Bandwidth: $\approx 10\%$



Replacing the *wire element* with a *planar element*

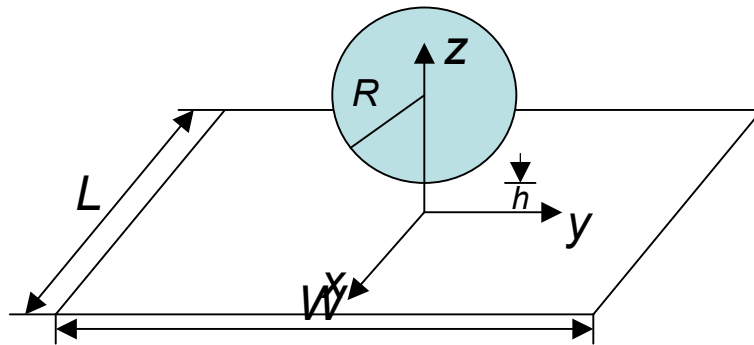


UWB

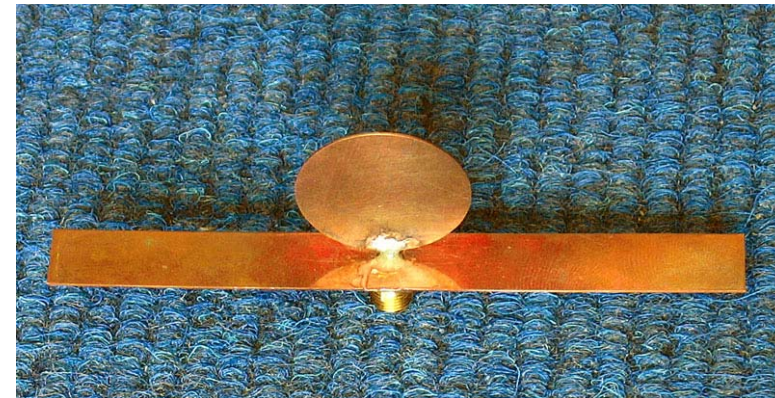
Monopoles

Circular disc monopole--

Vertical type



Geometry of the antenna



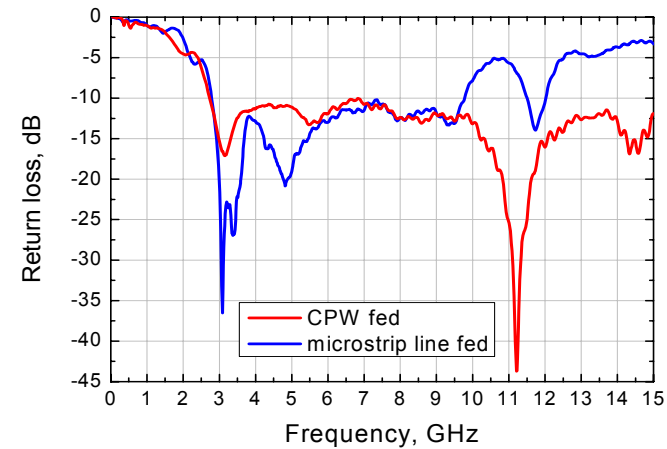
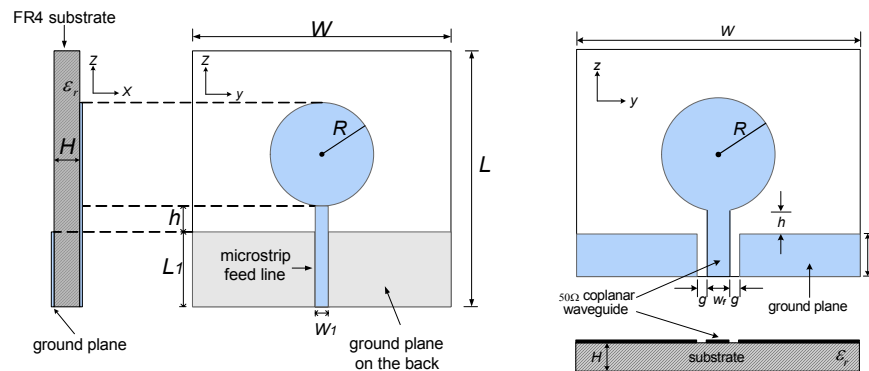
$R=12.5\text{mm}$, $h=0.7\text{mm}$, $W=100\text{mm}$ and $L=10\text{mm}$

wide bandwidth, satisfactory radiation properties,
simple structure, low cost

Non-planar

Planar Monopoles

- Optimising the topology of planar antennas to reduce antenna size while retaining UWB.
- CPW-fed disc was found has a better impedance matching over microstrip-fed disc monopole.

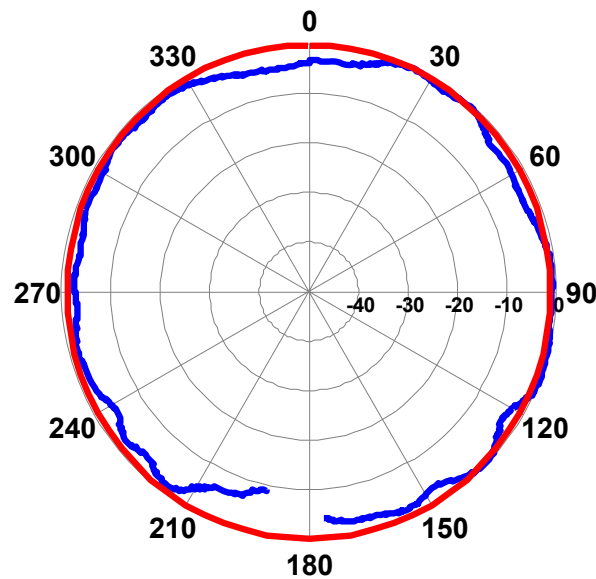


47mm×41mm with a dielectric constant of 4.7

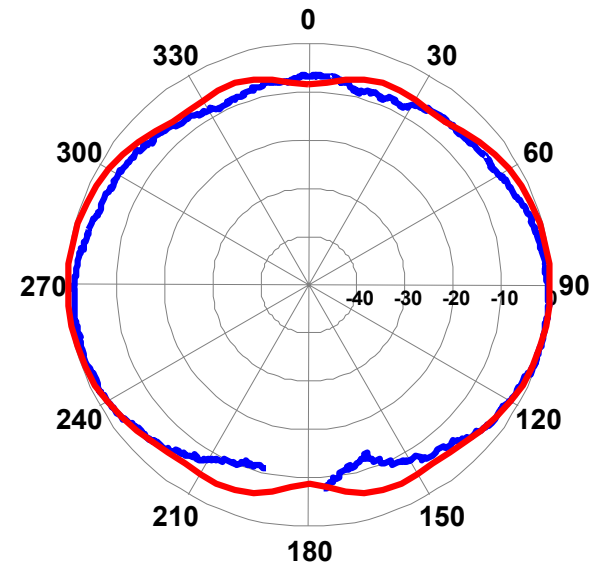
CPW fed (2.73GHz-15GHz)
Microstrip fed (2.78GHz-9.78GHz)

Radiation Patterns – CPW fed

- The H -plane pattern of the CPW-Fed disc monopole antenna is omni-directional at 3 GHz but distorted at 8.8 GHz



At 3 GHz

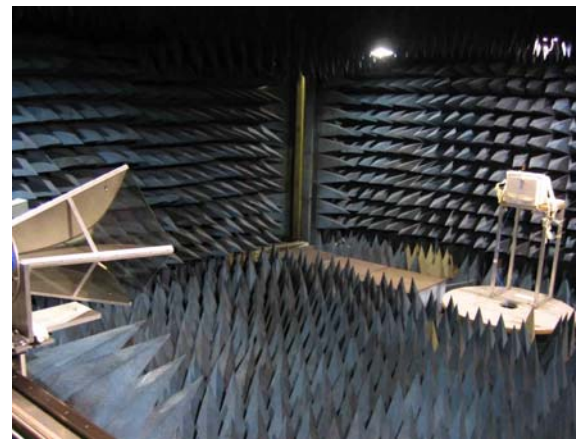
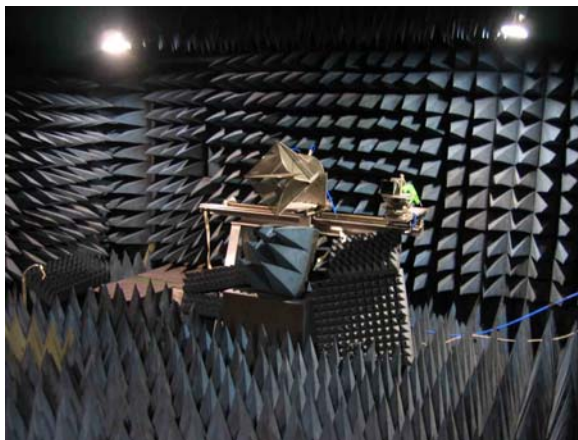
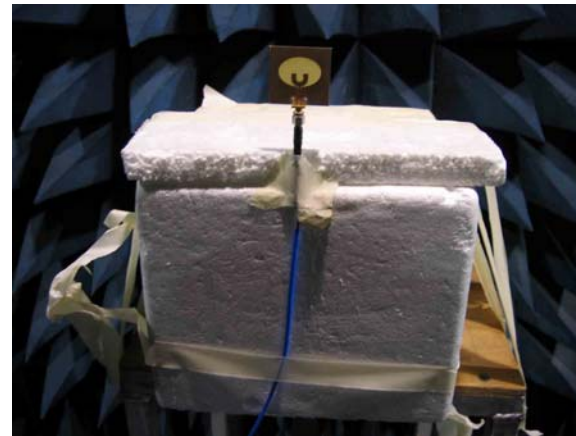
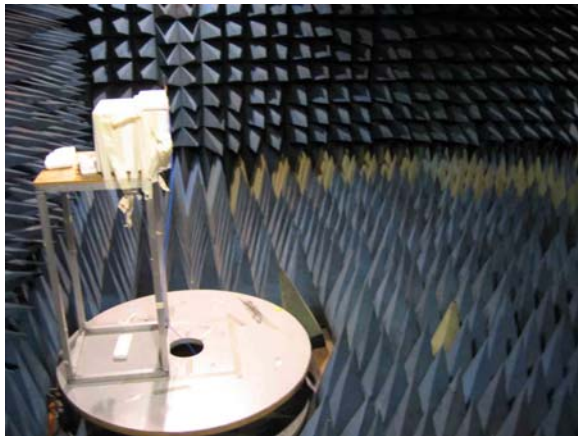


At 8.8 GHz

The simulated (red line) and measured (blue line) H -plane radiation patterns of CPW-Fed disc monopole antenna

Measurement of Monopoles

➤ Measurement set-up



Mechanism of UWB monopoles

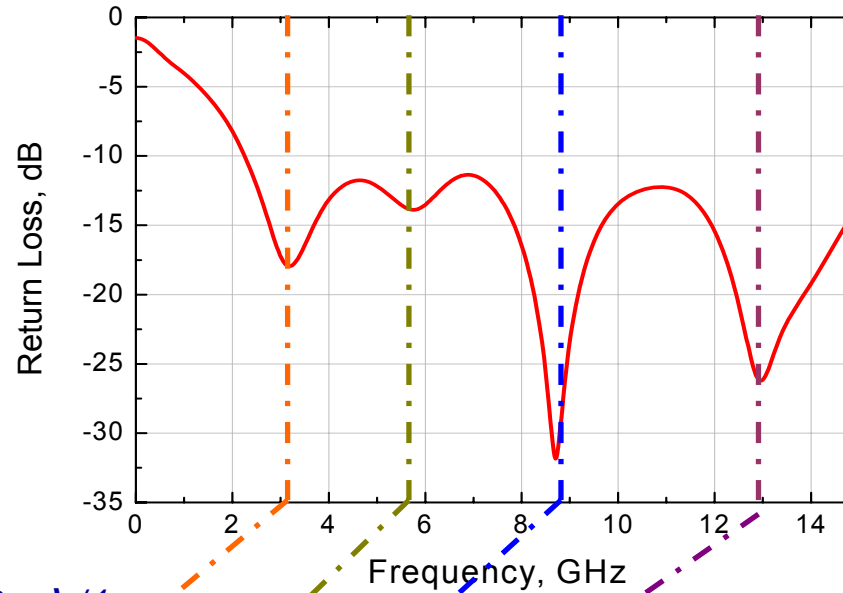
- How exactly a printed UWB monopole operates across the entire bandwidth?

Does a planar UWB monopole break Chu-Harrington's limit?

Mechanism of UWB monopoles

The disc supports multiple resonant modes

Simulated return loss curves



First resonant freq:

$$2R \approx \lambda_1 / 4$$

Second resonant freq:

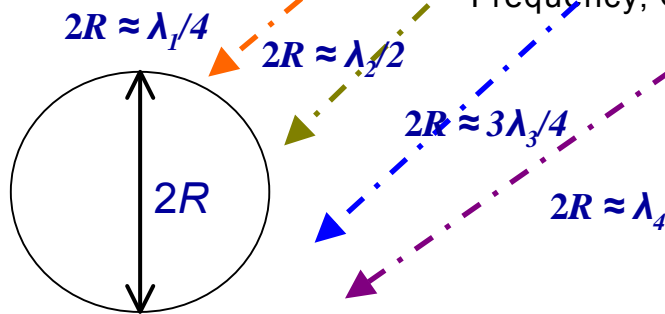
$$2R \approx \lambda_2 / 2$$

Third resonant freq:

$$2R \approx 3\lambda_3 / 4$$

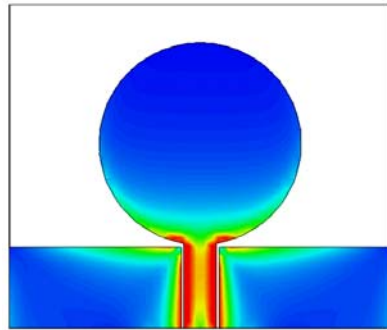
Forth resonant freq:

$$2R \approx \lambda_4$$

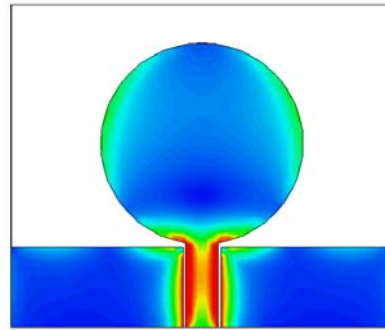


Mechanism of UWB monopoles

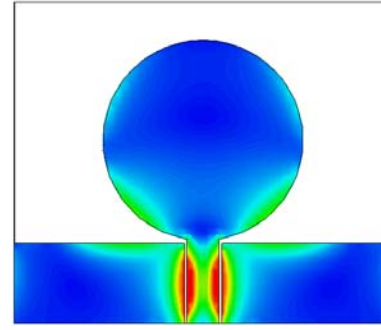
Current distribution



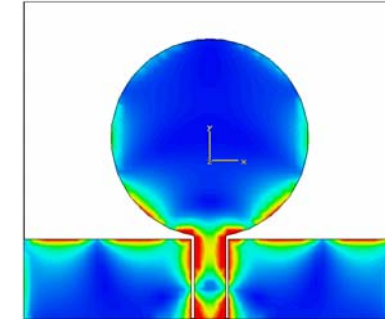
At 3GHz



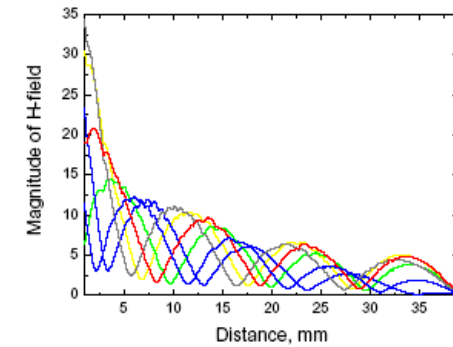
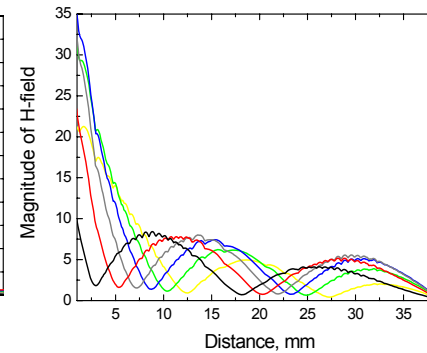
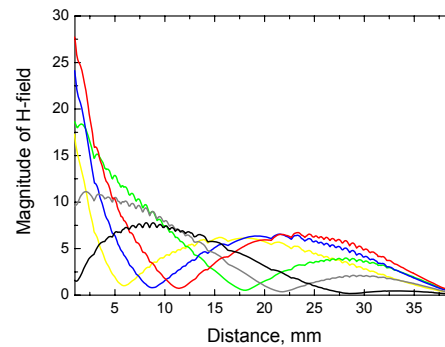
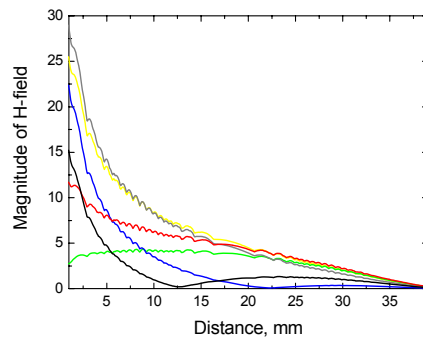
At 5.6GHz



At 8.6GHz



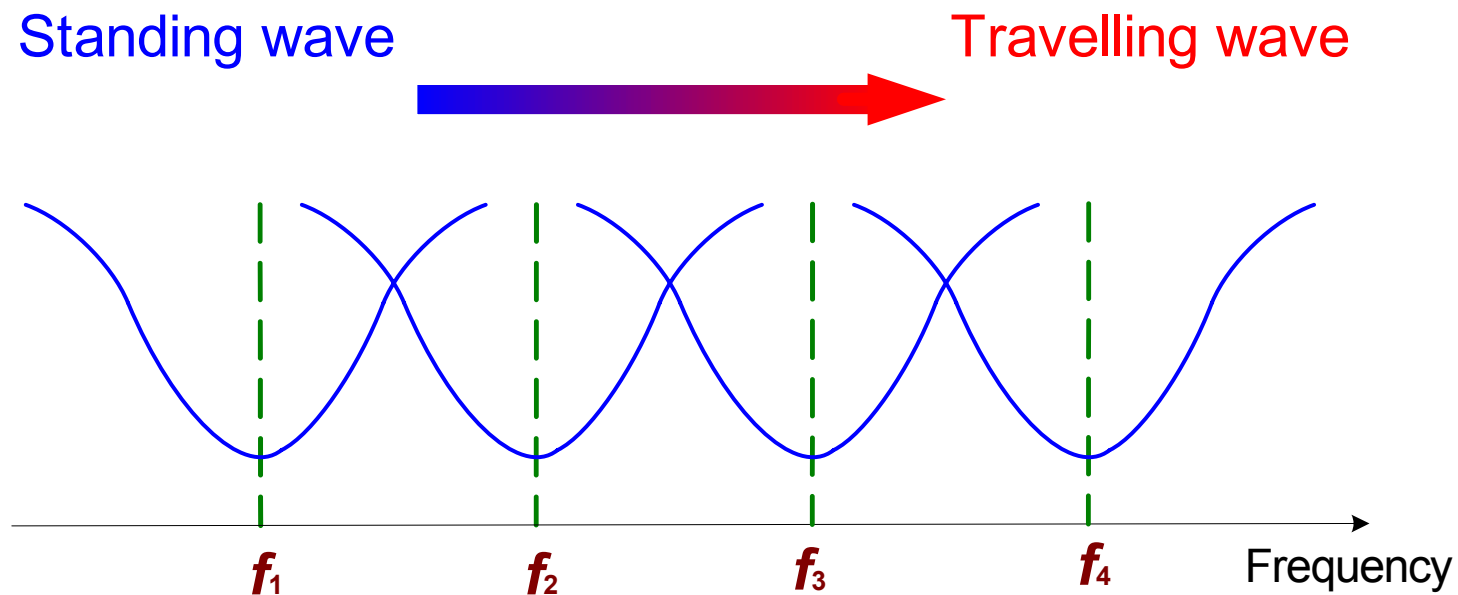
At 12.8GHz



H-field distributions along the edge of the half disc

Mechanism of UWB monopoles

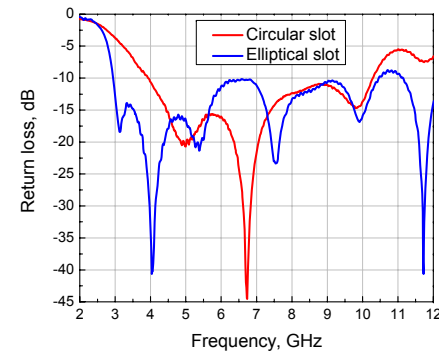
- Hybrid mode: standing wave + travelling wave
- Good feeding structure for traveling wave at high freq.



Slot Monopoles

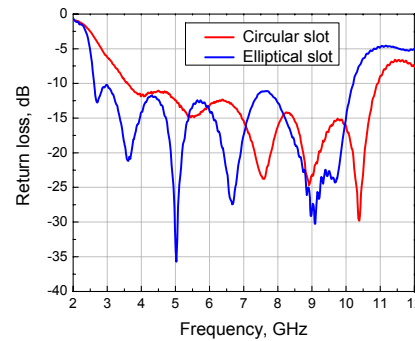
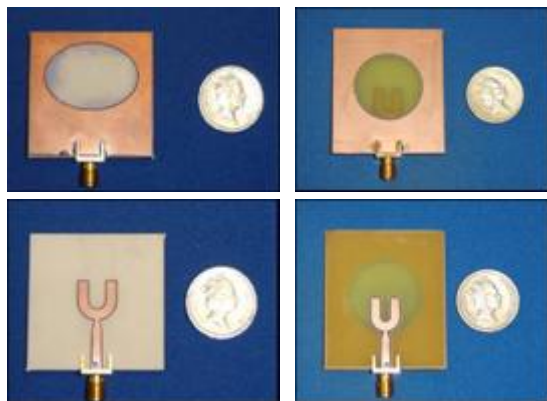
➤ Elliptical / circular slot antennas

CPW-fed:

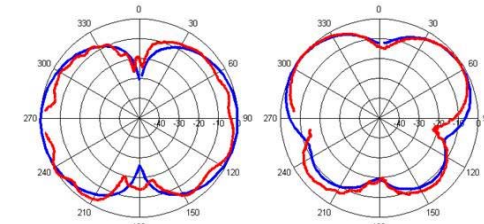


Measured return loss

Microstrip line fed:

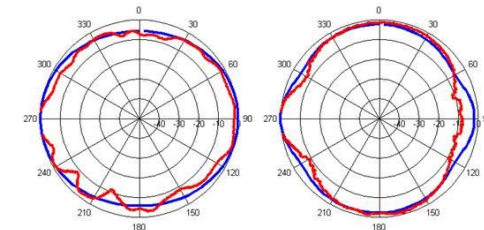


Measured return loss



E-Plane pattern

At 3.1GHz At 10GHz



H-Plane pattern

Half Monopoles

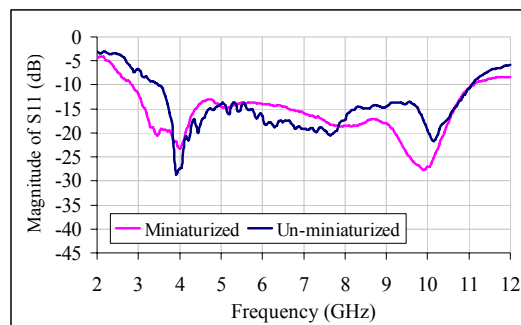
- Halve the disc antennas to achieve a 40% reduction in size.
- The miniaturisation improves the impedance bandwidth but reduces the gain and degrades the polarization purity in the upper frequency range.

Original size:
17×17 mm with a LTCC
dielectric constant of 7.8

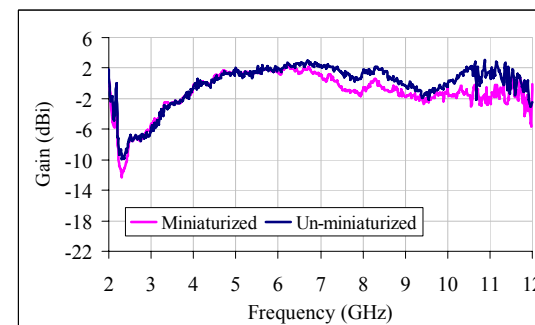


Reduced size:
10×17 mm with a LTCC
dielectric constant of 7.8

iWAT'07, M. Sun, Y.P. Zhang, NTU, Singapore



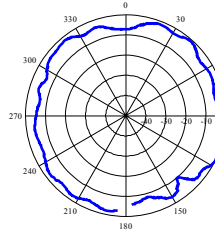
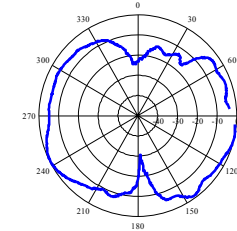
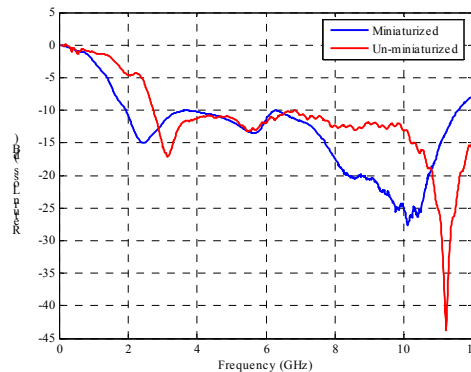
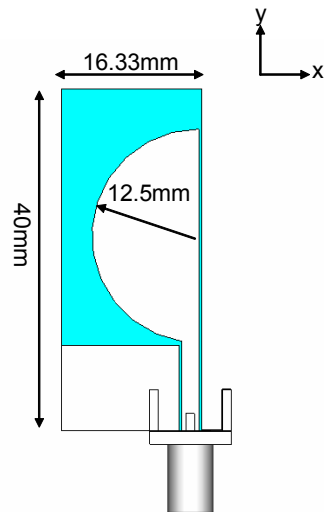
Measured return losses



Measured gain

Half Monopoles

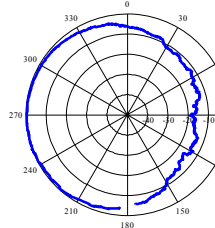
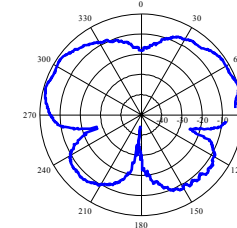
- In QMUL, The CPW-fed disc monopole was cut into half, the reduced antenna size is 16.33×40 mm with a dielectric constant of 3.
- The return loss is below -10 dB within 1.94-11.59GHz frequency band.



E-Plane pattern

At 2.45GHz

At 5.64GHz



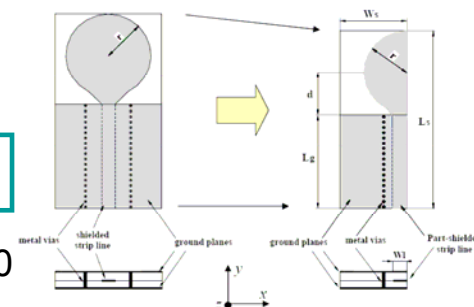
H-Plane pattern

Measured return losses

half disc- blue line Full disc – red line

A similar design was proposed by B. Sanz-Izquierdo and J.C. Batchelor, University of Kent, LAPC 2007

37 x 20mm



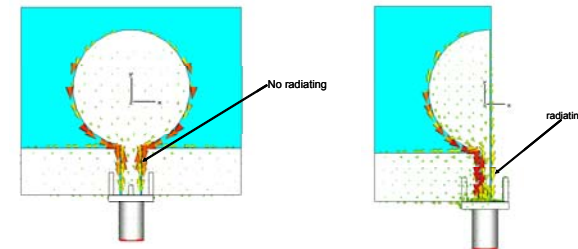
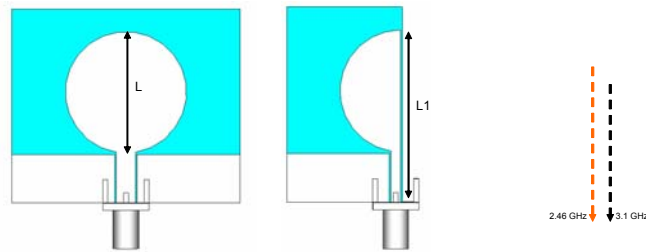
34.25 x 12.5mm

29th Nov 20

19

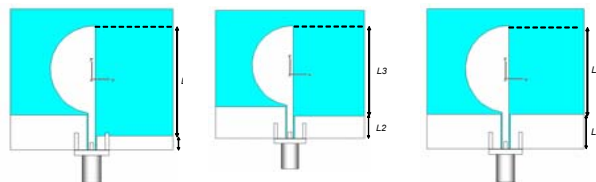
Half Monopoles

➤ Mechanism of the miniaturized antenna



Firstly, the disc monopole antenna is simply chopped half

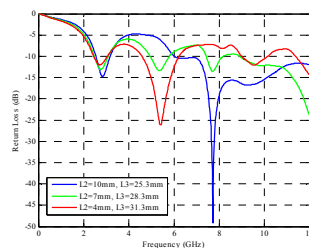
Current distributions



The relationships between $L2$, $L3$ and the first resonances

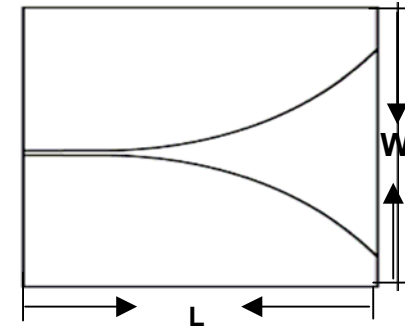
Further verification by introducing a ground plane on the other side with different length $L2$

	$L2=4\text{mm},$ $L3=31.3\text{mm}$	$L2=7\text{mm},$ $L3=28.3\text{mm}$	$L2=10\text{mm},$ $L3=25.3\text{mm}$	$L=25\text{ mm}$ (full disc)
First Resonance $f1$	2.72 GHz	2.76 GHz	2.84 GHz	3.01 GHz
wavelength λ at $f1$	110.3mm	108.7mm	105.6mm	99.7mm
$L3/\lambda$	0.28	0.26	0.24	0.25

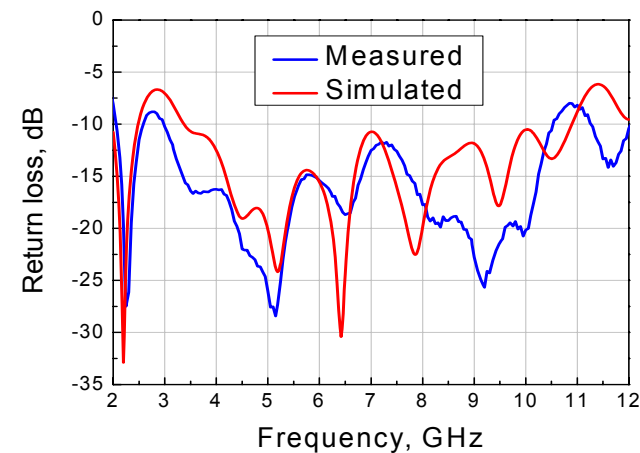


Tapered Slot Antennas

- As a travelling wave antenna, TSA has demonstrated multi-octave bandwidth.
- A typical TSA should have a aperture width of slot $W \geq \lambda_0/2$ and the length of the TSA L from 2 to $12\lambda_0$.
- It is not suitable for application when low-profile is essential.



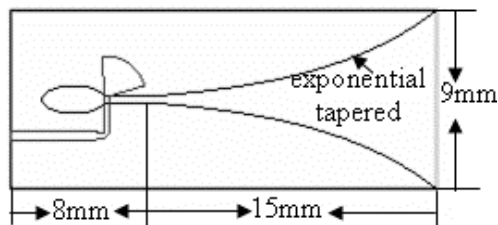
70.6mm×60mm



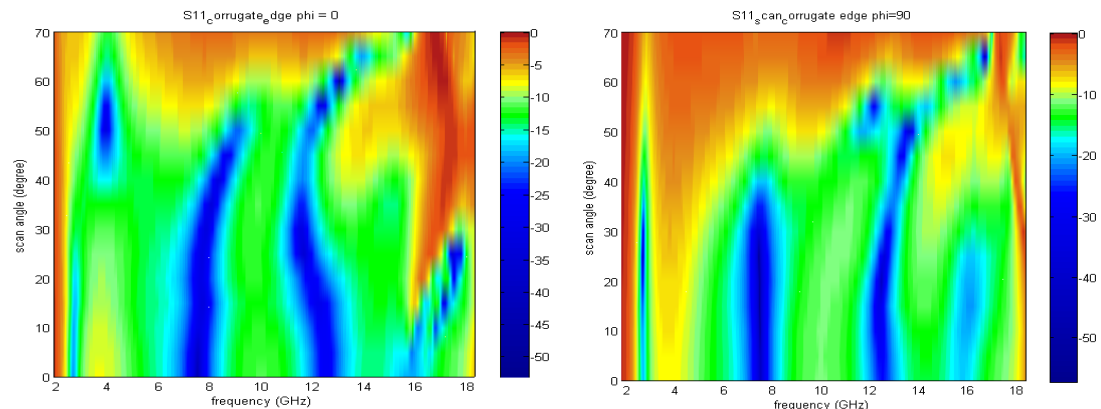
Measured: 3.3GHz—10.8GHz
Simulated: 3.0GHz—10.5GHz

Miniature Tapered Slot Array Antenna

- The miniature tapered slot antenna in an array environment can obtain a bandwidth of 4-16GHz with wide scan angle. The element is only 0.12λ in width and 0.3λ in depth at 4GHz.
- The wideband impedance matching is achieved essentially due to the constructive effect of the mutual coupling among elements.



23mm×9mm



E- and H-plane Scanned Active Reflection Coefficient (dB) of the TSA array as the function of scan angle Θ and frequency. The bandwidth achieved is approaching 4:1 from 4-16GHz

Conclusions

- Planar monopoles are capable of supporting multiple resonance modes, overlapping of the evenly spaced modes leads to UWB characteristic – Chu-Harington limit no longer hold in multiple resonances!
- A remarkable more than 50% size reduction can be achieved for printed disc monopole antenna for UWB systems by simply halving the original antenna and tuning other parameters
- The small tapered slot antenna can achieve wideband performance in an array environment due to strong mutual coupling between elements.

Q&A



Thank You